



Federal Environmental, Industrial and Nuclear Supervision Service

Scientific and Engineering Centre
for Nuclear and Radiation Safety



EUROSAFE | 2019

ETSON

EUROPEAN
TECHNICAL SAFETY
ORGANISATIONS
NETWORK

Actual issues of VVER reactor pressure vessel irradiation embrittlement assessment

Dr. Alexander Kryukov

OUTLINE

Introduction

OUTLINE

Introduction

RPV Radiation Damage

OUTLINE

Introduction

RPV Radiation Damage

Irradiation Embrittlement Mitigation by Annealing

OUTLINE

Introduction

RPV Radiation Damage

Irradiation Embrittlement Mitigation by Annealing

VVER RPV-440 life time long term operation

OUTLINE

Introduction

RPV Radiation Damage

Irradiation Embrittlement Mitigation by Annealing

VVER RPV-440 life time long term operation

International STRUMAT project

TYPICAL PWR RPV



▶ Vessels may weigh up to 800t with wall thickness up to ~330mm.

WWER-440 RPV



REACTOR PRESSURE VESSELS

- Cannot be replaced

REACTOR PRESSURE VESSELS

- Cannot be replaced
- Under high pressure, temperature and radiation:

REACTOR PRESSURE VESSELS

- Cannot be replaced
- Under high pressure, temperature and radiation:
 - pressure: 12-18 MPa,

REACTOR PRESSURE VESSELS

- Cannot be replaced
- Under high pressure, temperature and radiation:
 - pressure: 12-18 MPa,
 - temperature: 270 - 325 °C,

REACTOR PRESSURE VESSELS

- Cannot be replaced
- Under high pressure, temperature and radiation:
 - pressure: 12-18 MPa,
 - temperature: 270 - 325 °C,
 - neutron fluence: $10^{17} \text{ cm}^{-2} - 3 \times 10^{20} \text{ cm}^{-2}$ ($E > 0.5 \text{ MeV}$)

REACTOR PRESSURE VESSELS

- Cannot be replaced
- Under high pressure, temperature and radiation:
 - pressure: 12-18 MPa,
 - temperature: 270 - 325 °C,
 - neutron fluence: $10^{17} \text{ cm}^{-2} - 3 \times 10^{20} \text{ cm}^{-2}$ ($E > 0.5 \text{ MeV}$)
- Effects of several stressors from operating conditions

AGEING STRUCTURE



STRESSORS

stress-constant

strain constant

stress variable
strain variable

temperature

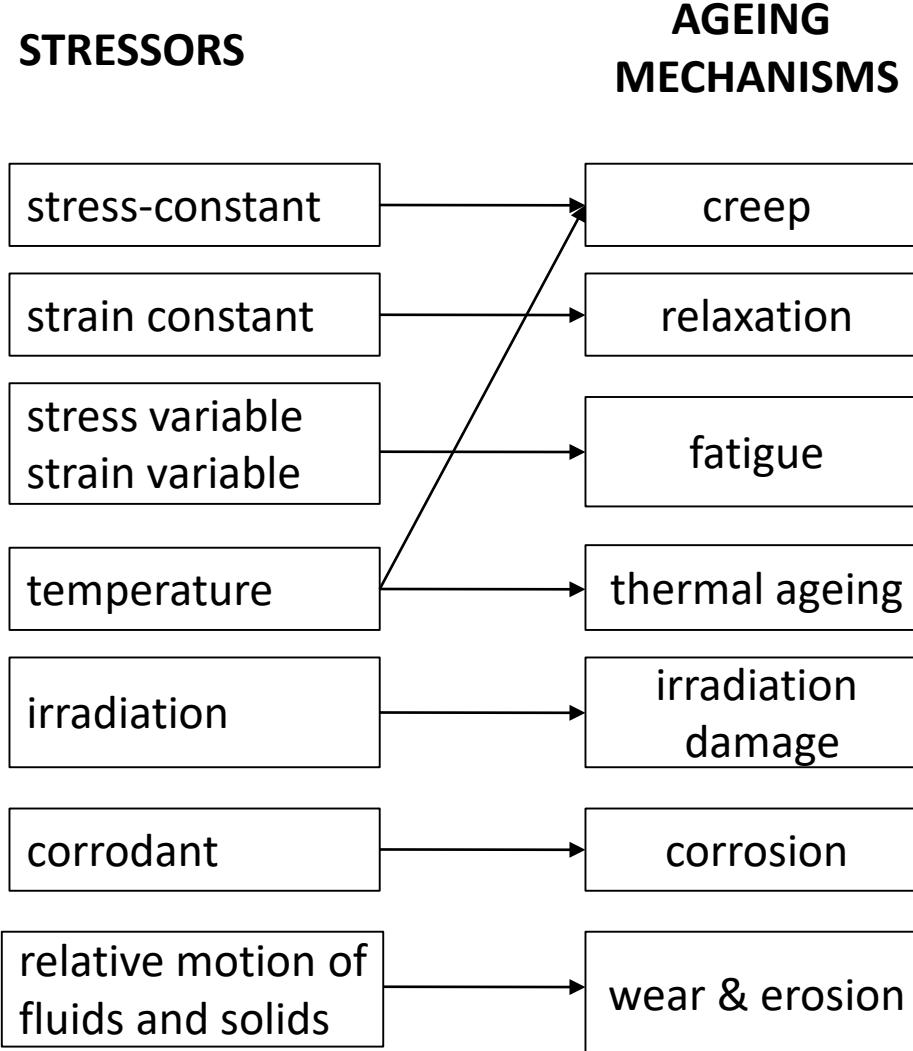
irradiation

corrodant

relative motion of
fluids and solids

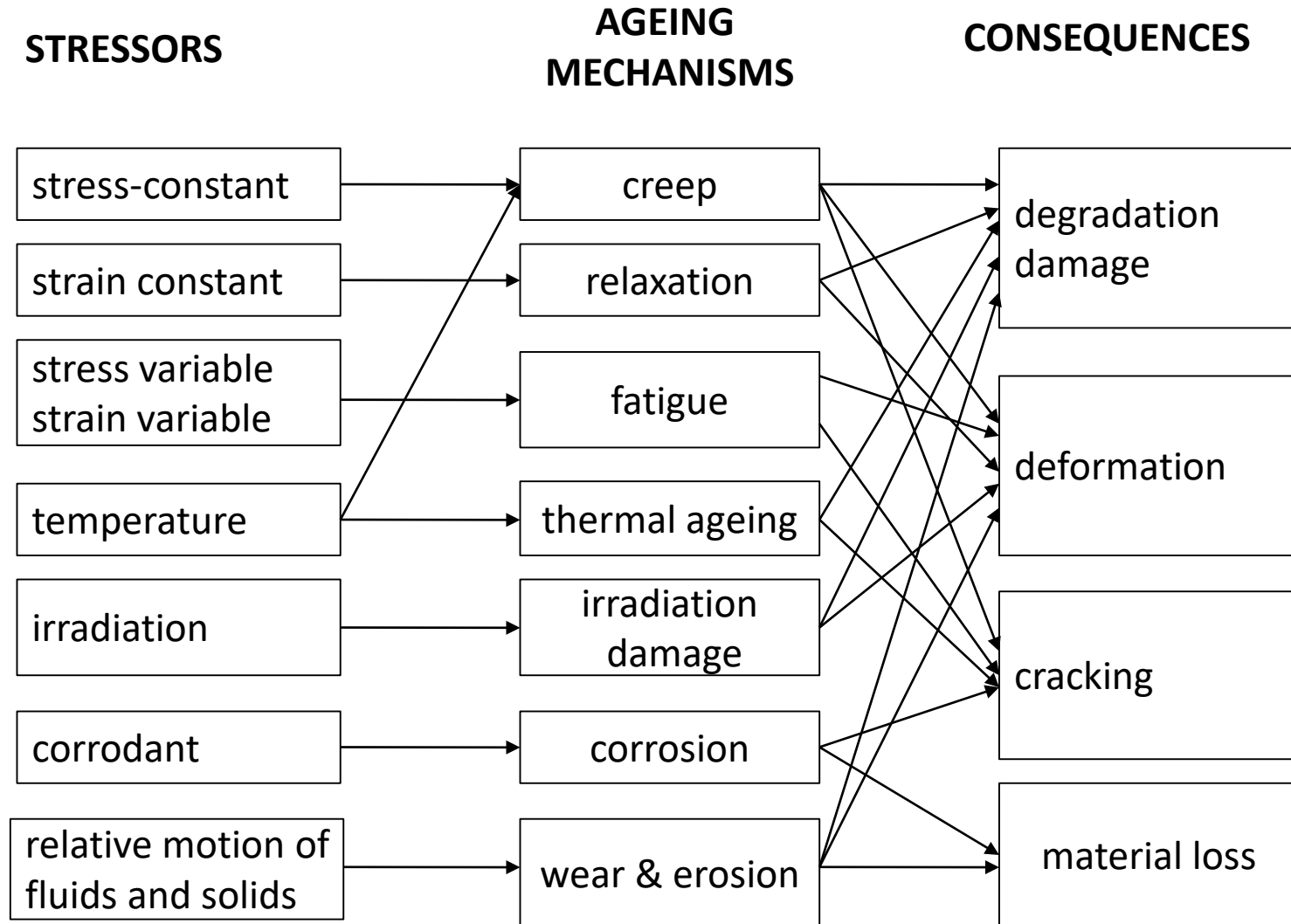
A major stressor in an ageing structure is time itself

AGEING STRUCTURE



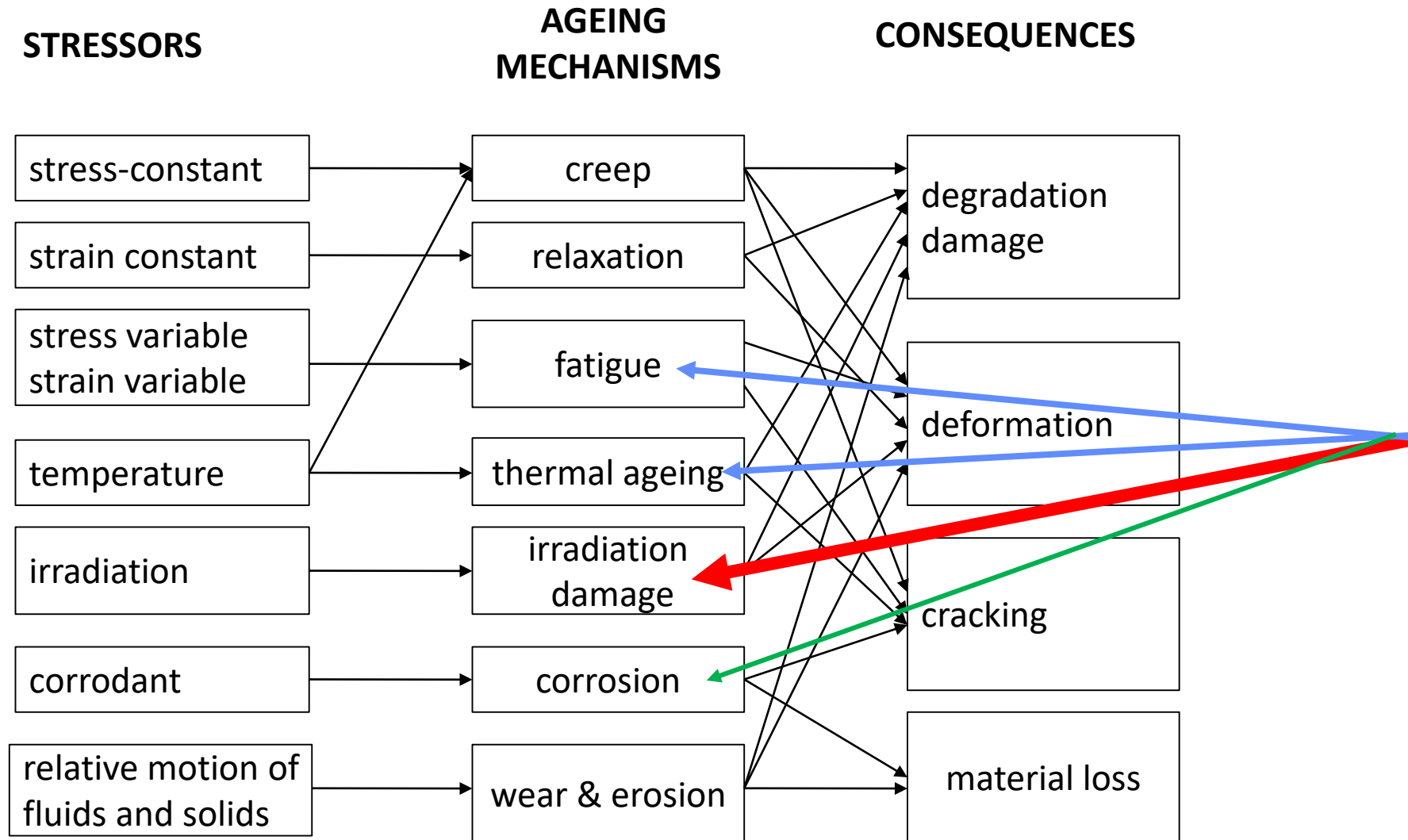
A major stressor in an ageing structure is time itself

AGEING STRUCTURE



A major stressor in an ageing structure is time itself

AGEING STRUCTURE



A major stressor in an ageing structure is time itself

RADIATION DAMAGE (Irradiation Embrittlement)

Most important ageing mechanism resulting to:

RADIATION DAMAGE (Irradiation Embrittlement)

Most important ageing mechanism resulting to:

- Increase in strength properties

RADIATION DAMAGE (Irradiation Embrittlement)

Most important ageing mechanism resulting to:

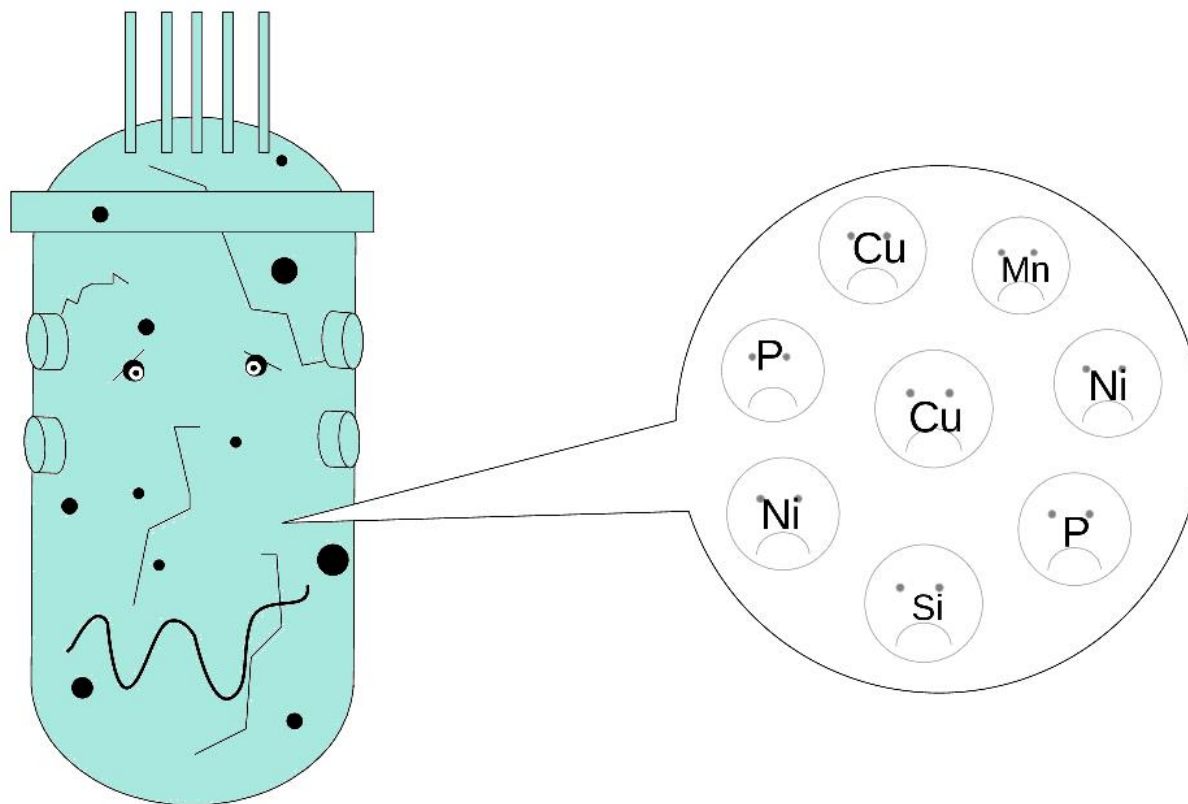
- Increase in strength properties
- Decrease in ductility and reduction of area

RADIATION DAMAGE (Irradiation Embrittlement)

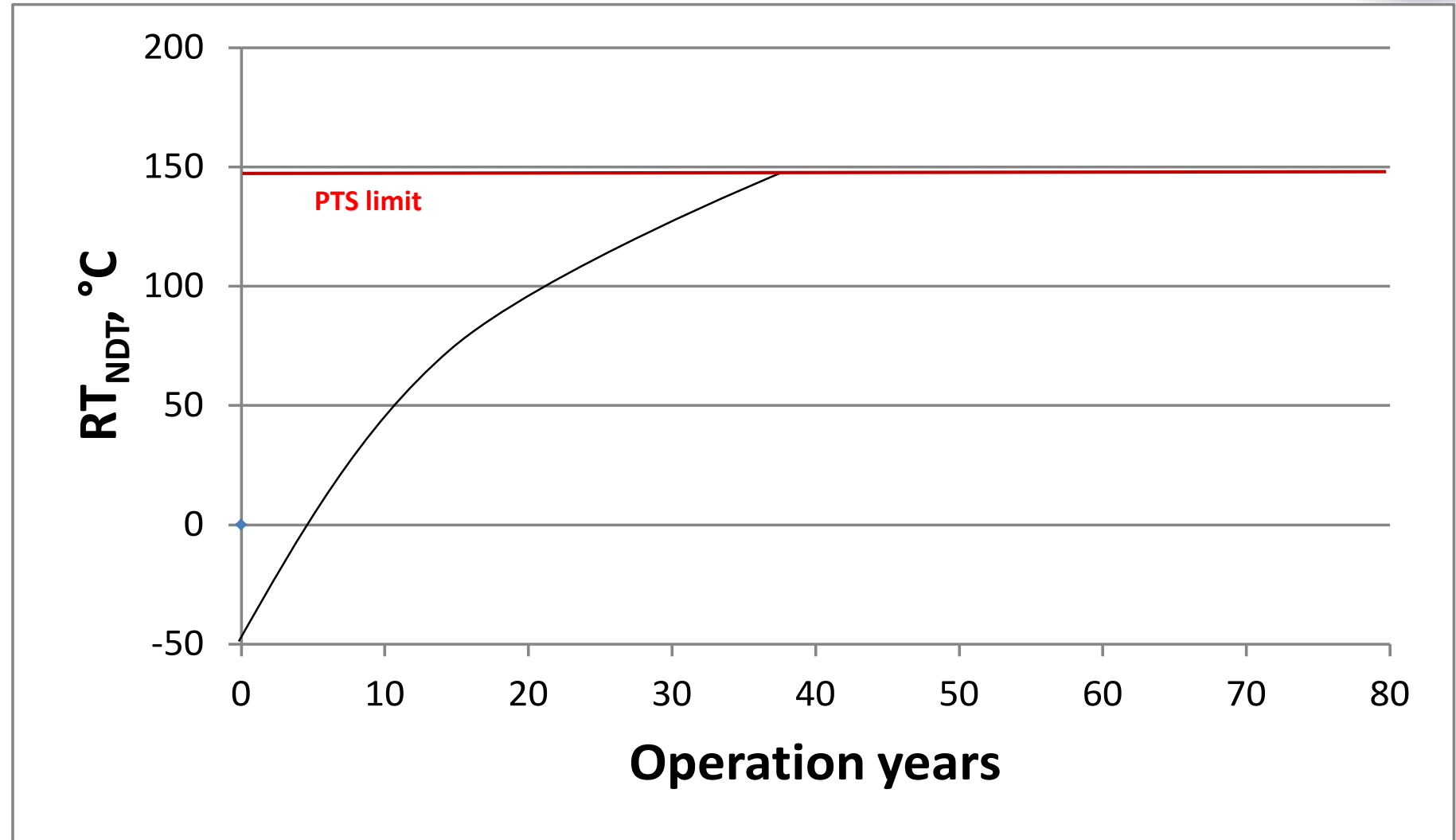
Most important ageing mechanism resulting to:

- Increase in strength properties
- Decrease in ductility and reduction of area
- Shift of impact and fracture toughness dependences to higher temperatures

Main influencing elements: Cu, P, Ni and Mn



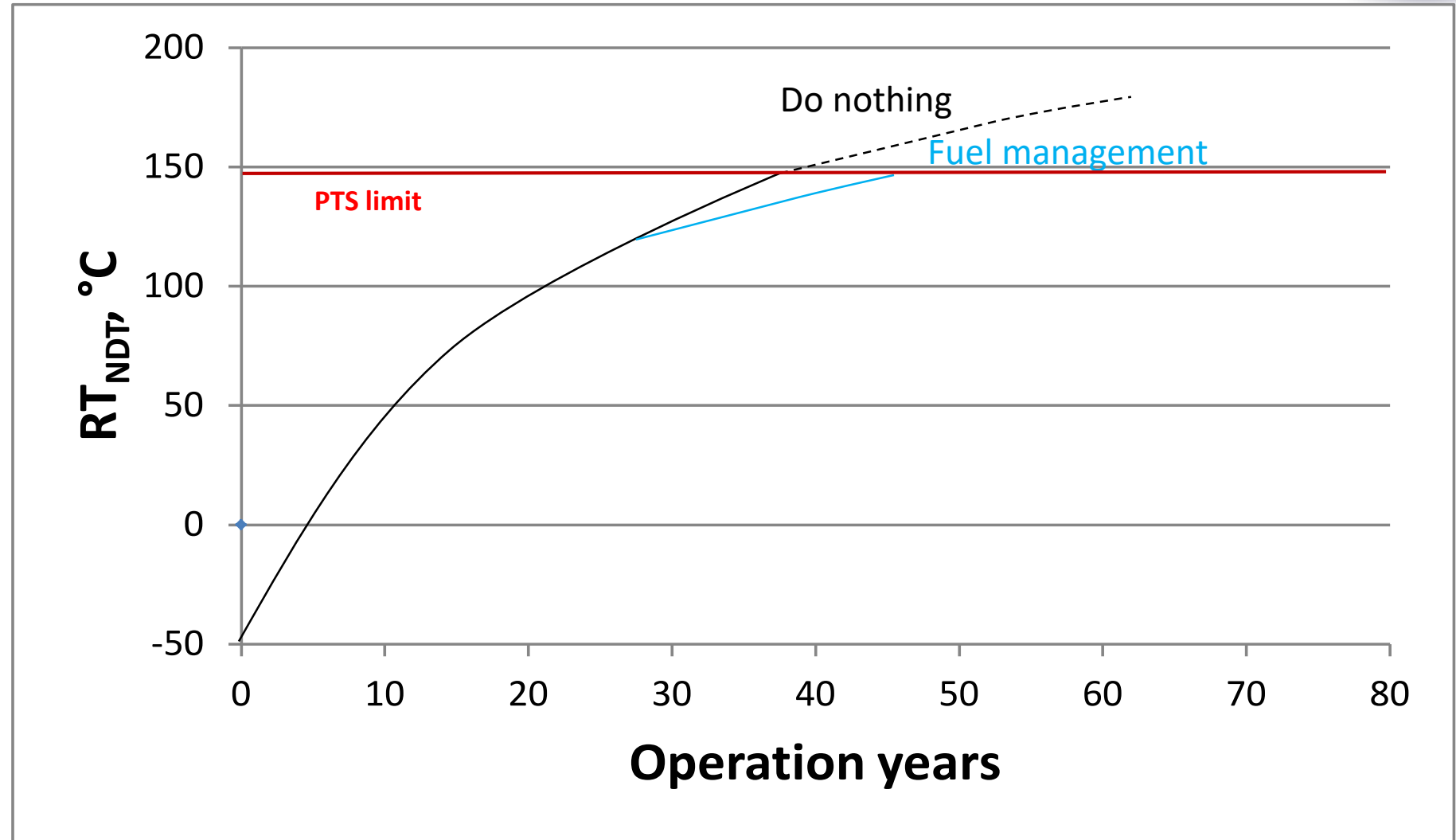
RPV ageing management



RPV ageing management



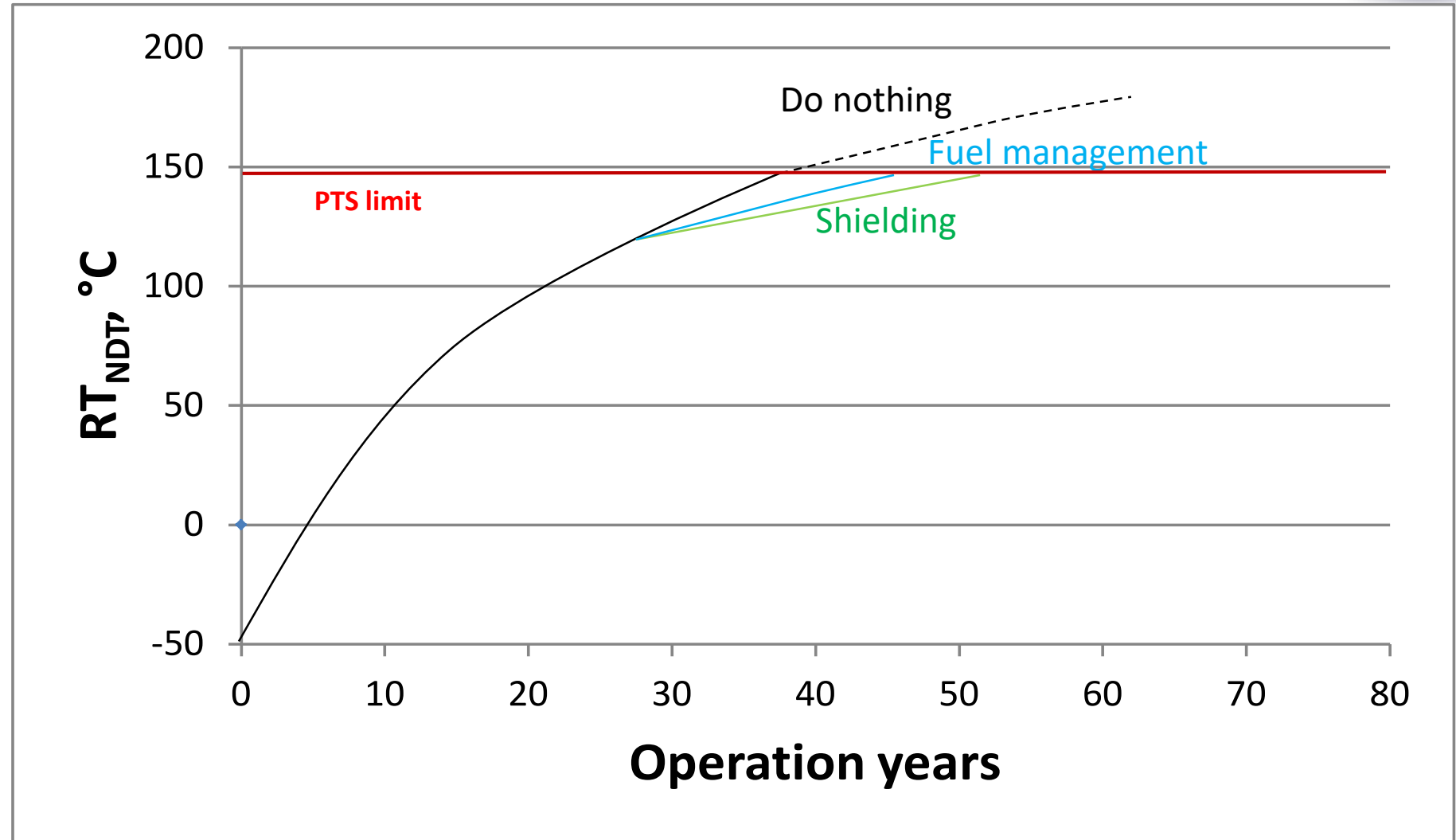
- Fuel management



RPV ageing management



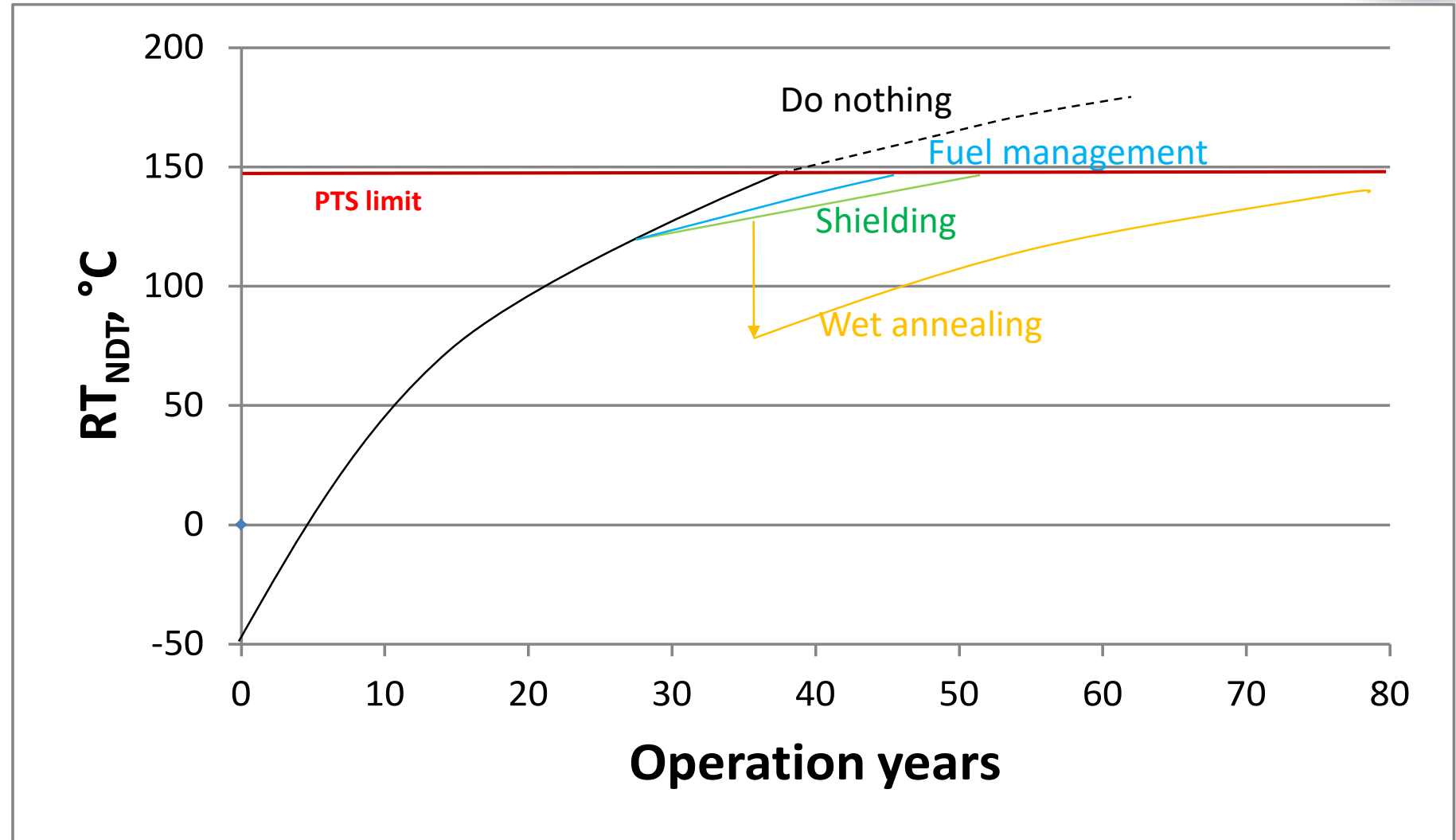
- Fuel management
- RPV shielding



RPV ageing management



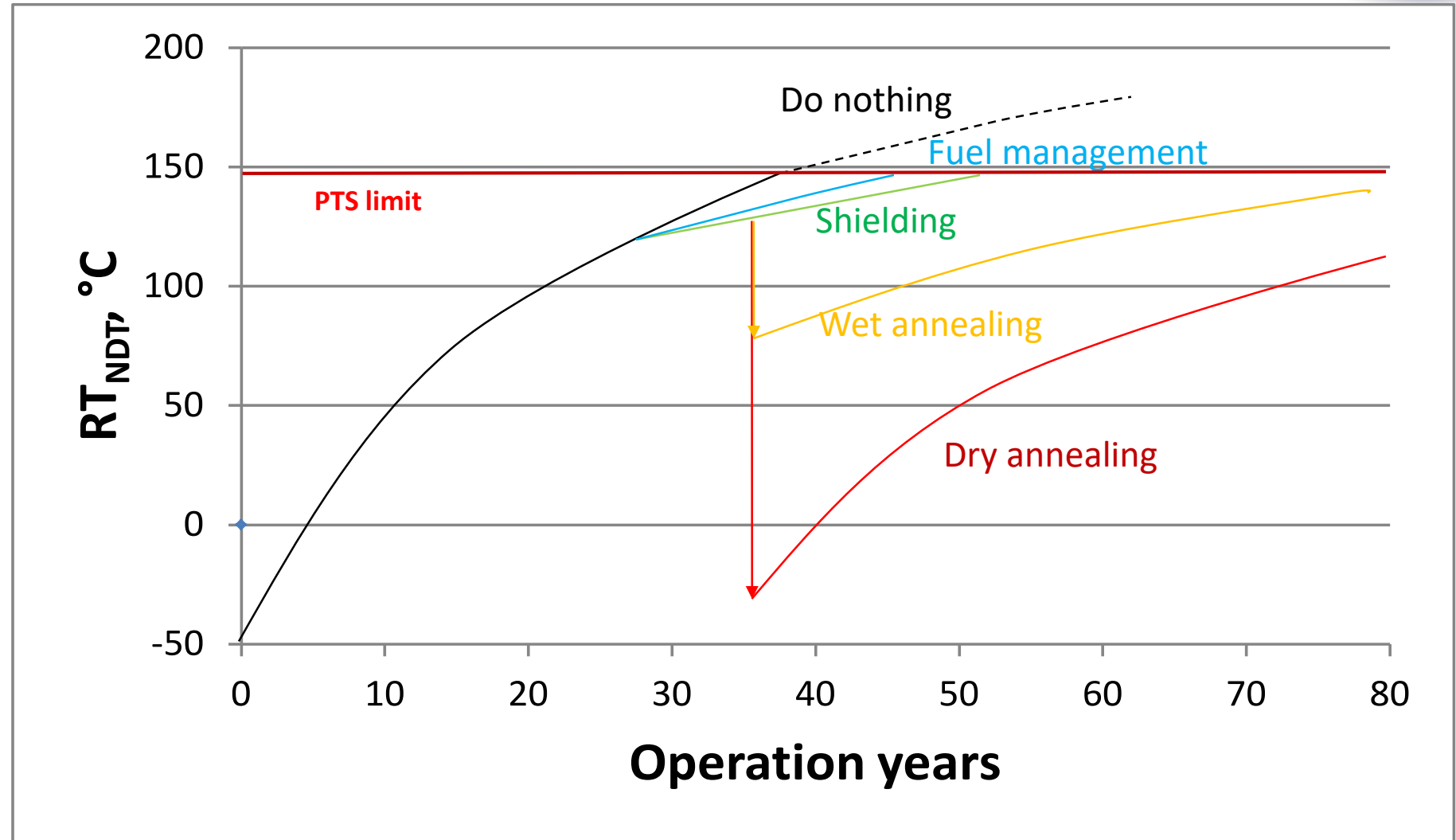
- Fuel management
- RPV shielding
- Thermal annealing
 - Wet annealing



RPV ageing management

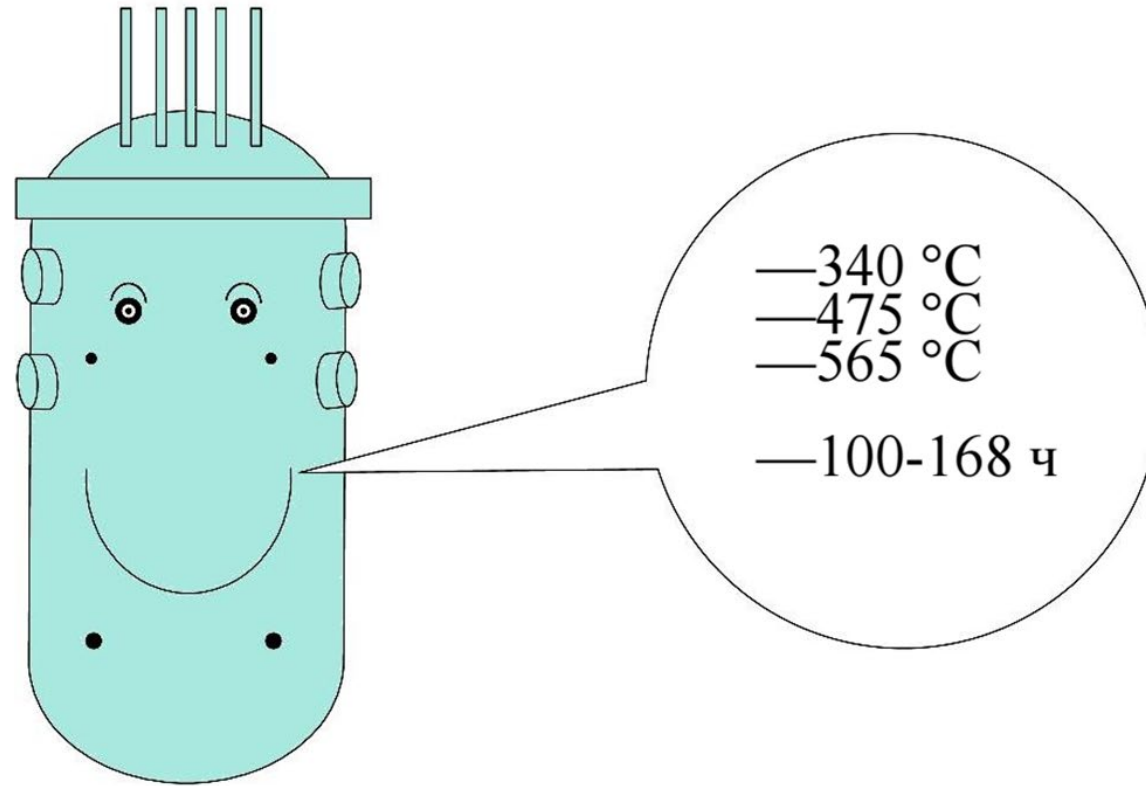


- Fuel management
- RPV shielding
- Thermal annealing
 - Wet annealing
 - Dry annealing



Annealing - most powerful solution

Irradiation embrittlement mitigation by thermal annealing



“Dry” annealing



High temperature ($> 400\text{ }^{\circ}\text{C}$)

“Dry” annealing



High temperature ($> 400\text{ }^{\circ}\text{C}$)

Removal of internals and primary water

“Dry” annealing



High temperature ($> 400\text{ }^{\circ}\text{C}$)

Removal of internals and primary water

Plant-specific evaluations for supports, primary coolant piping, pipe supports, concrete, insulation, etc.

“Dry” annealing

High temperature ($> 400\text{ }^{\circ}\text{C}$)

Removal of internals and primary water

Plant-specific evaluations for supports, primary coolant piping, pipe supports, concrete, insulation, etc.

20 VVER-440 RPVs annealed in 1987 - 2019 (Russia, Eastern Europe , Finland):
Standard regime: **460-490 $^{\circ}\text{C}$** , 100-168 hours

“Dry” annealing



High temperature ($> 400\text{ }^{\circ}\text{C}$)

Removal of internals and primary water

Plant-specific evaluations for supports, primary coolant piping, pipe supports, concrete, insulation, etc.

20 VVER-440 RPVs annealed in 1987 - 2019 (Russia, Eastern Europe , Finland):

Standard regime: $460\text{-}490\text{ }^{\circ}\text{C}$, 100-168 hours

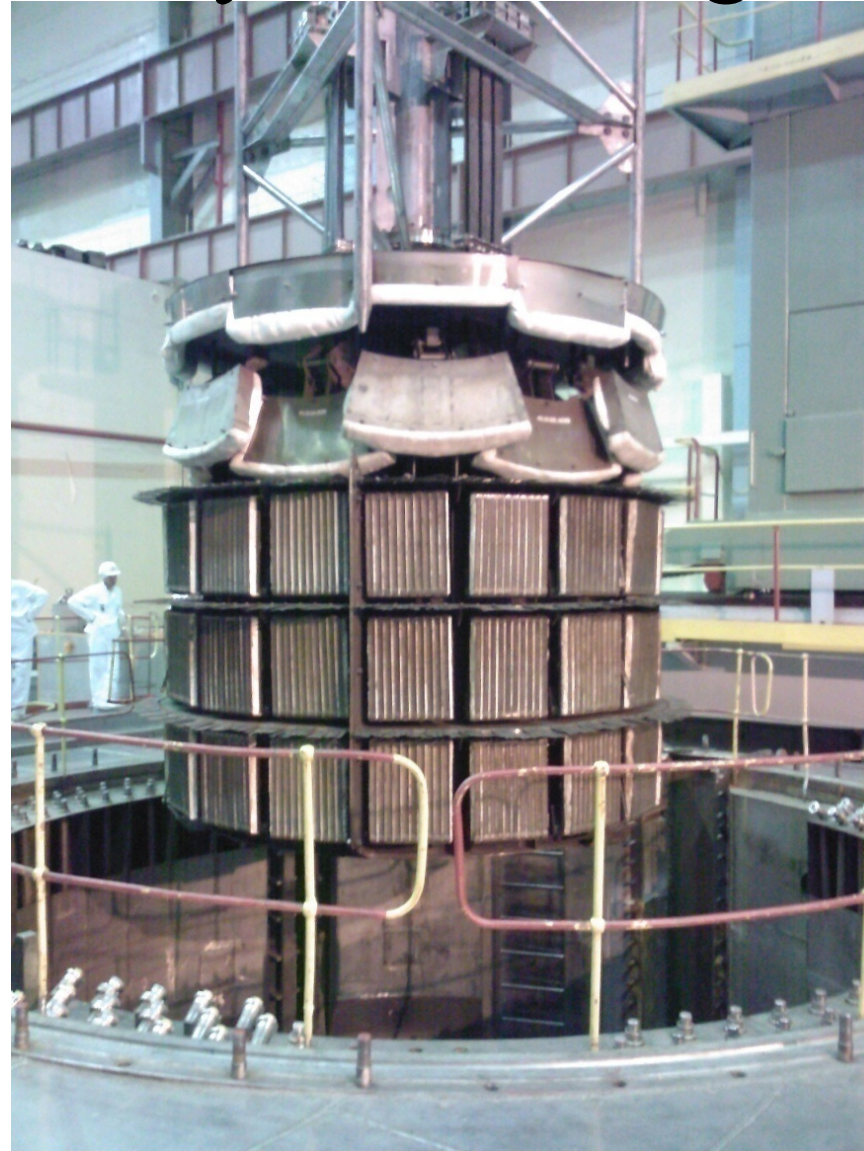
1st VVER-1000 RPV annealed in Russia in 2018:

$550\text{-}580\text{ }^{\circ}\text{C}$, 100 hours

“Dry” annealing



~20 RPV VVER, 1987 – 2019
(460-490 °C, 100-150 h.)



“Wet” annealing



- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure

“Wet” annealing

- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing

“Wet” annealing

- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing
- Reactor coolant water is heated by circulation pumps

“Wet” annealing

- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing
- Reactor coolant water is heated by circulation pumps
- **No need to remove internals from the reactor vessel**

“Wet” annealing

- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing
- Reactor coolant water is heated by circulation pumps
- **No need to remove internals from the reactor vessel**
- Wet annealing :
 - SM-1A (US Army, Alaska, 1967)

“Wet” annealing

- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing
- Reactor coolant water is heated by circulation pumps
- **No need to remove internals from the reactor vessel**
- Wet annealing :
 - SM-1A (US Army, Alaska, 1967)
 - BR3 (Belgium, 1984)

“Wet” annealing

- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing
- Reactor coolant water is heated by circulation pumps
- **No need to remove internals from the reactor vessel**
- Wet annealing :
 - SM-1A (US Army, Alaska, 1967)
 - BR3 (Belgium, 1984)
 - Both RPV welds contain high Cu contents

“Wet” annealing

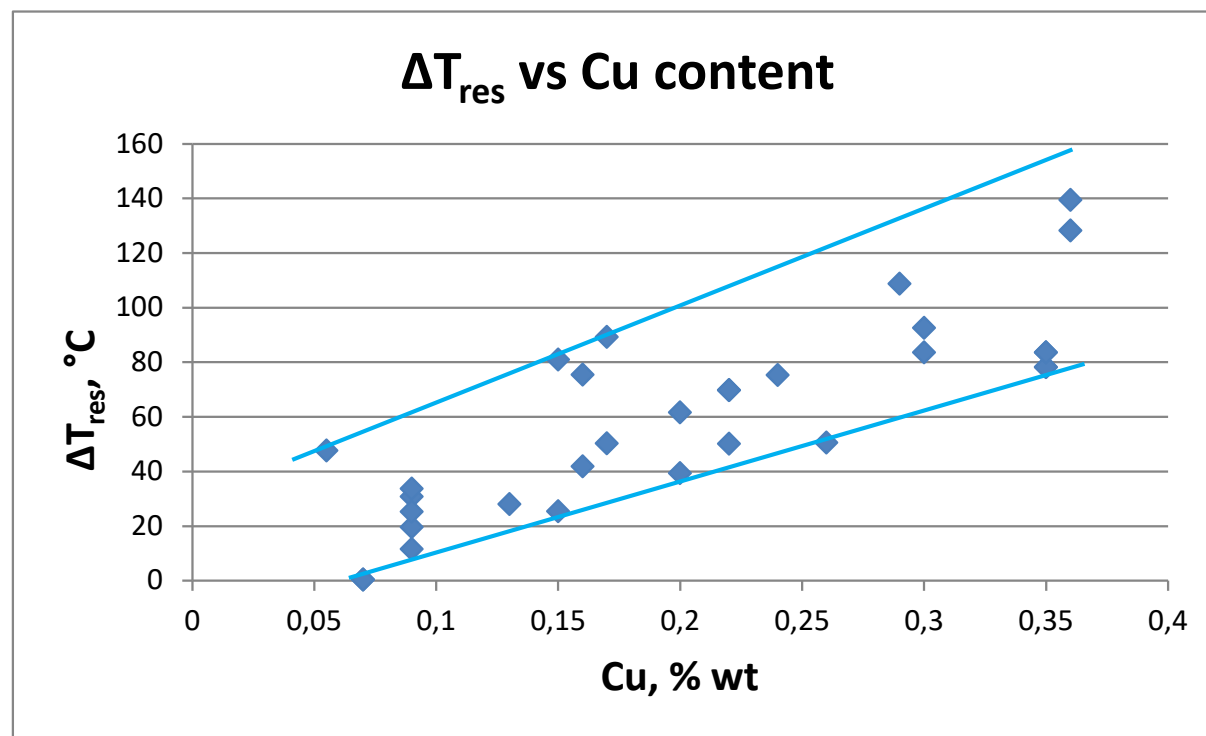
- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing
- Reactor coolant water is heated by circulation pumps
- **No need to remove internals from the reactor vessel**
- Wet annealing :
 - SM-1A (US Army, Alaska, 1967)
 - BR3 (Belgium, 1984)
 - Both RPV welds contain high Cu contents
- Recovery of mechanical properties $\sim 20\text{-}40\%$

“Wet” annealing

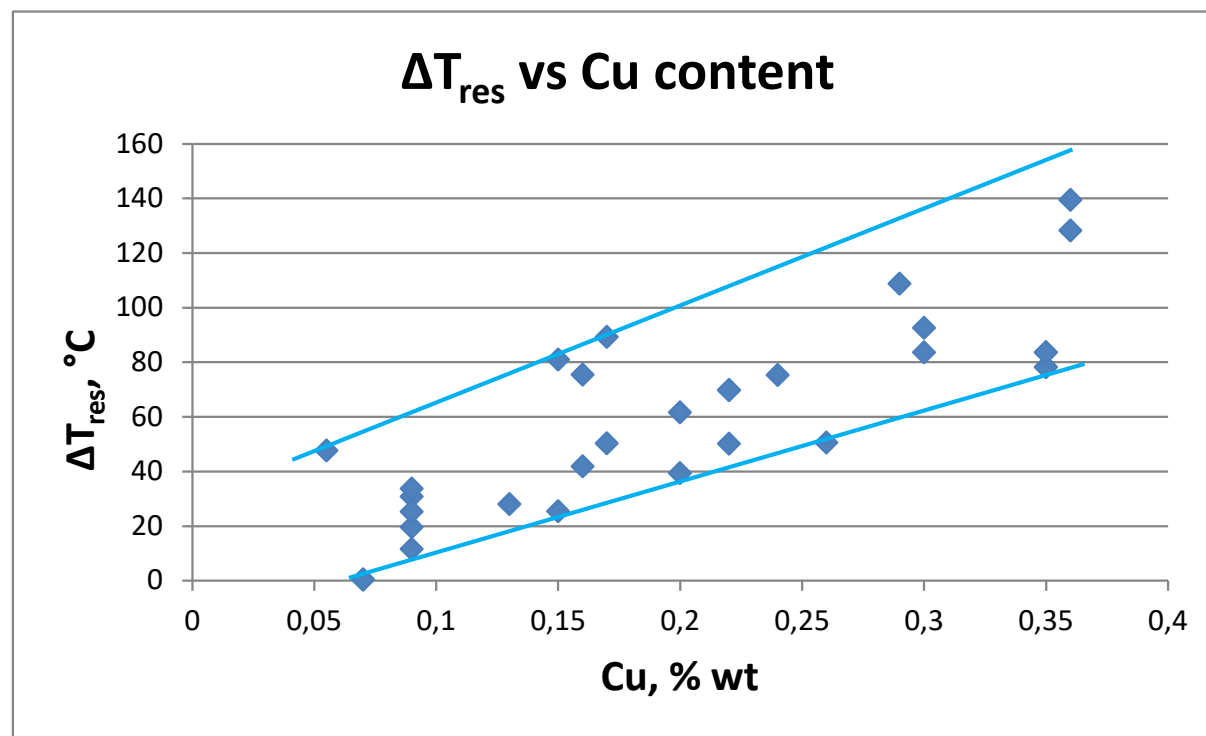
- Temperatures $\leq 343^{\circ}\text{C}$ based on maximum allowable pressure
- Very much less expensive and complicated than “dry” annealing
- Reactor coolant water is heated by circulation pumps
- **No need to remove internals from the reactor vessel**
- Wet annealing :
 - SM-1A (US Army, Alaska, 1967)
 - BR3 (Belgium, 1984)
 - Both RPV welds contain high Cu contents
- Recovery of mechanical properties $\sim 20\text{-}40\%$

Conclusion in the 80s – “wet” annealing is not effective for high Cu steels

Residual after annealing (at 343°C) T_k shift depends on Cu content (PWR steels)

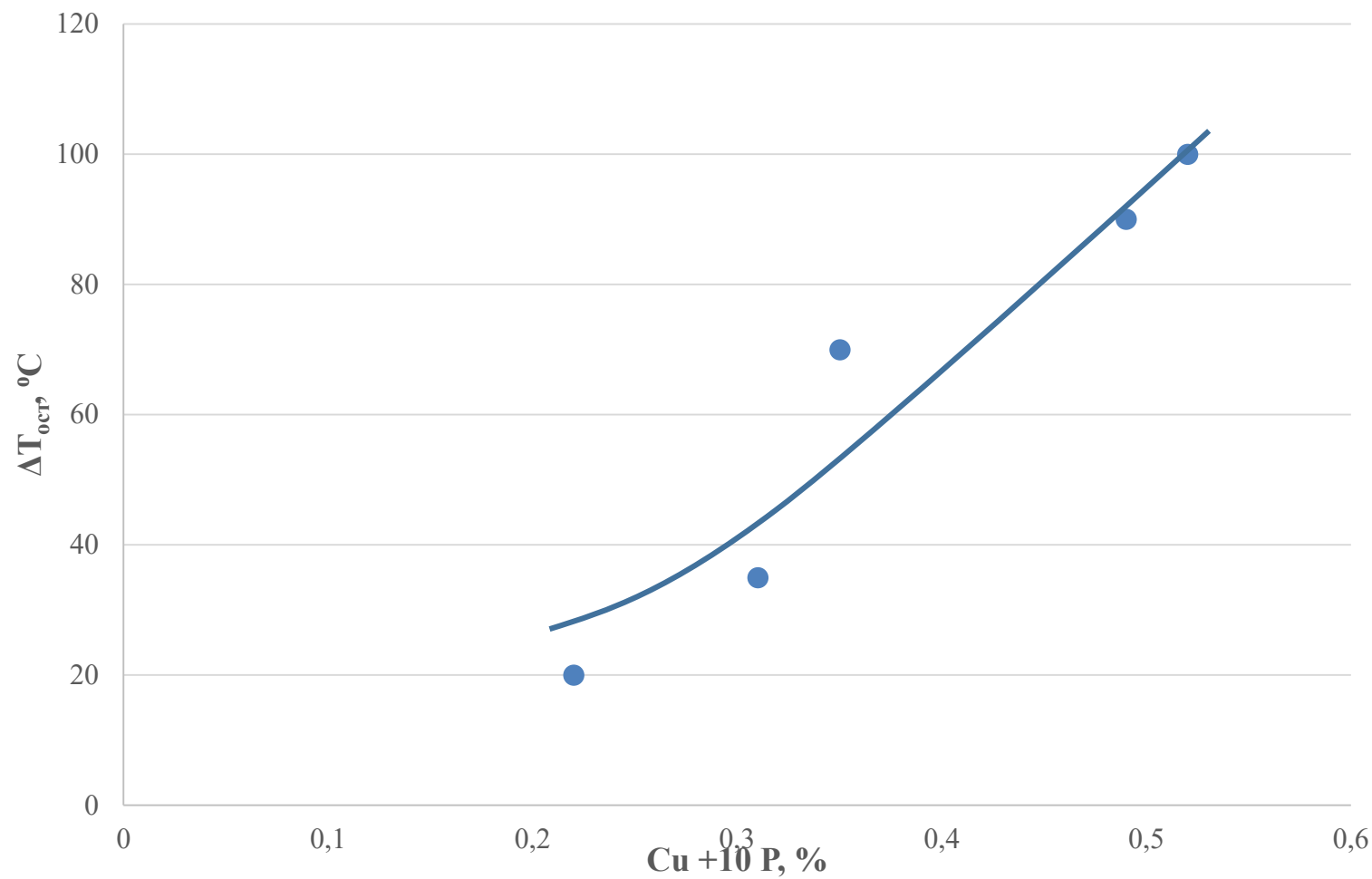


Residual after annealing (at 343°C) T_k shift depends on Cu content (PWR steels)

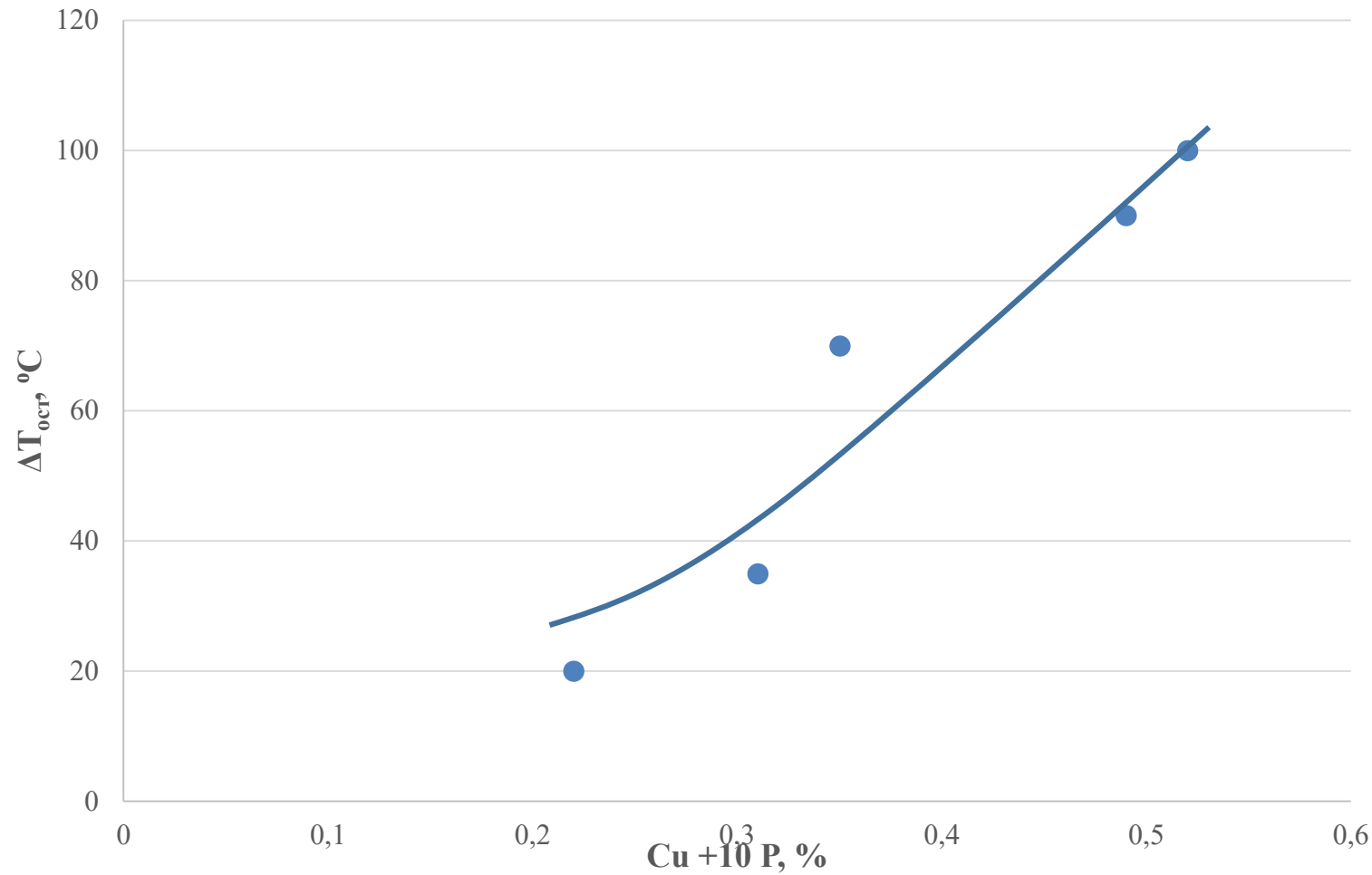


Wet annealing is effective for low Cu PWR RPV steels

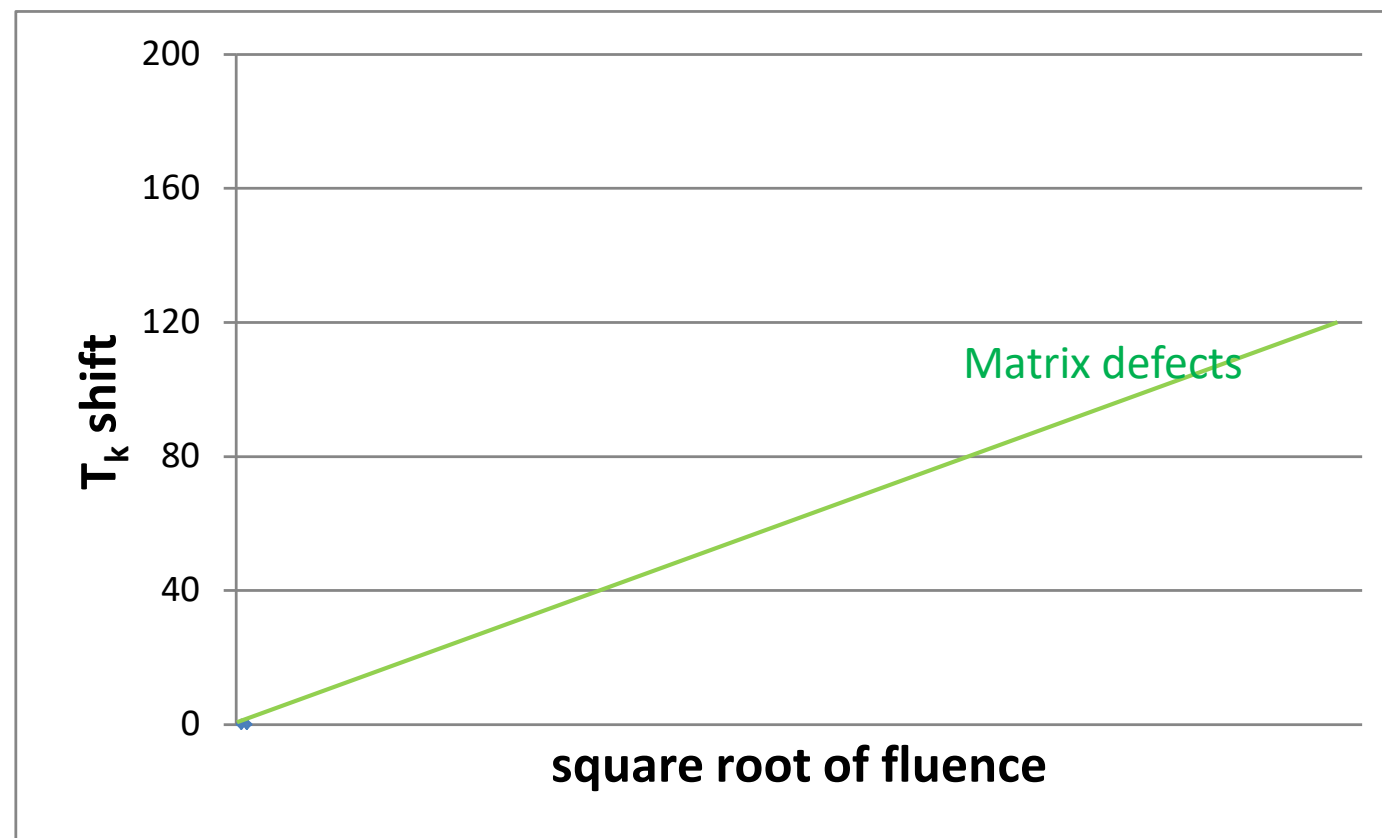
Residual after annealing (at 340°C) T_k shift depends on Cu & P content (VVER steels)



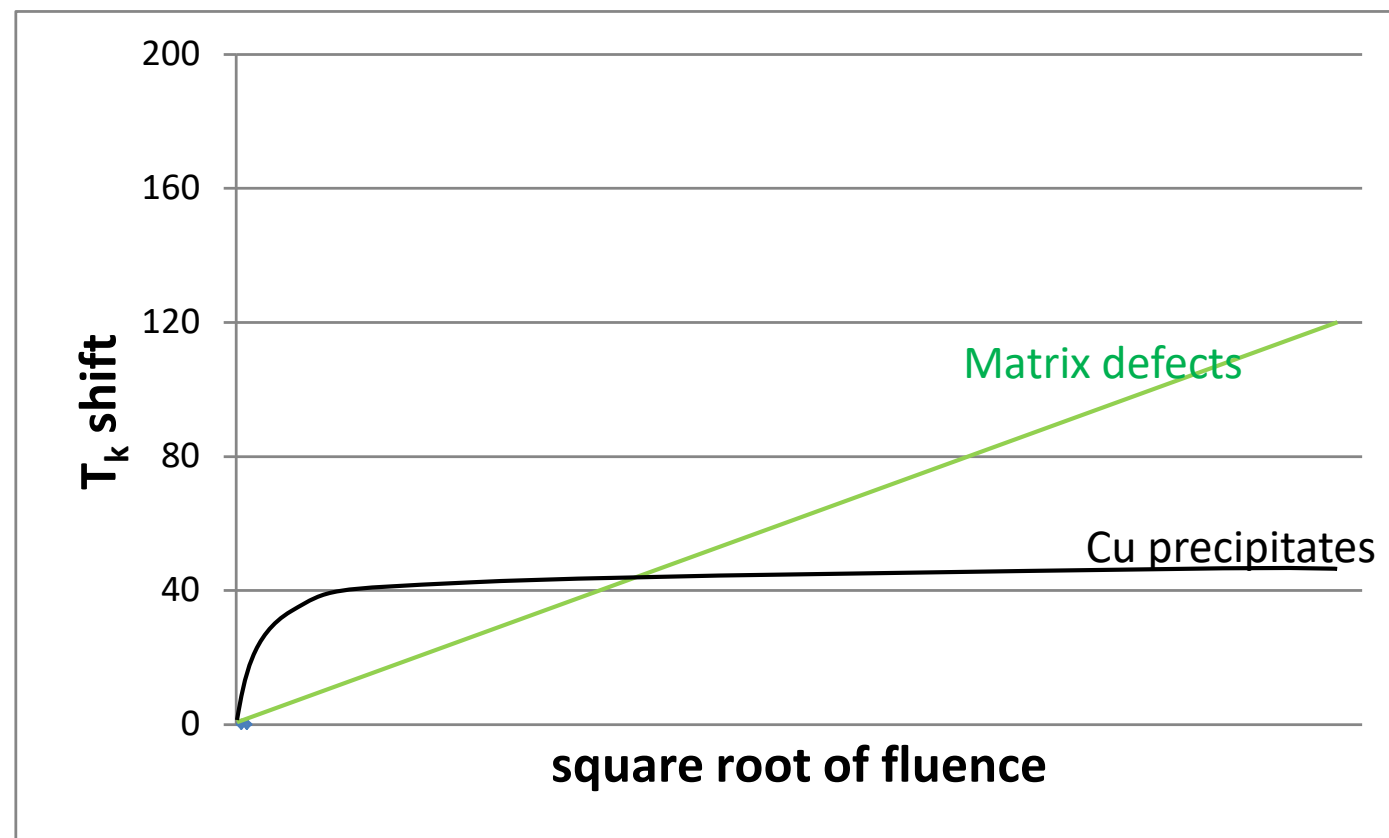
Residual after annealing (at 340°C) T_k shift depends on Cu & P content (VVER steels)



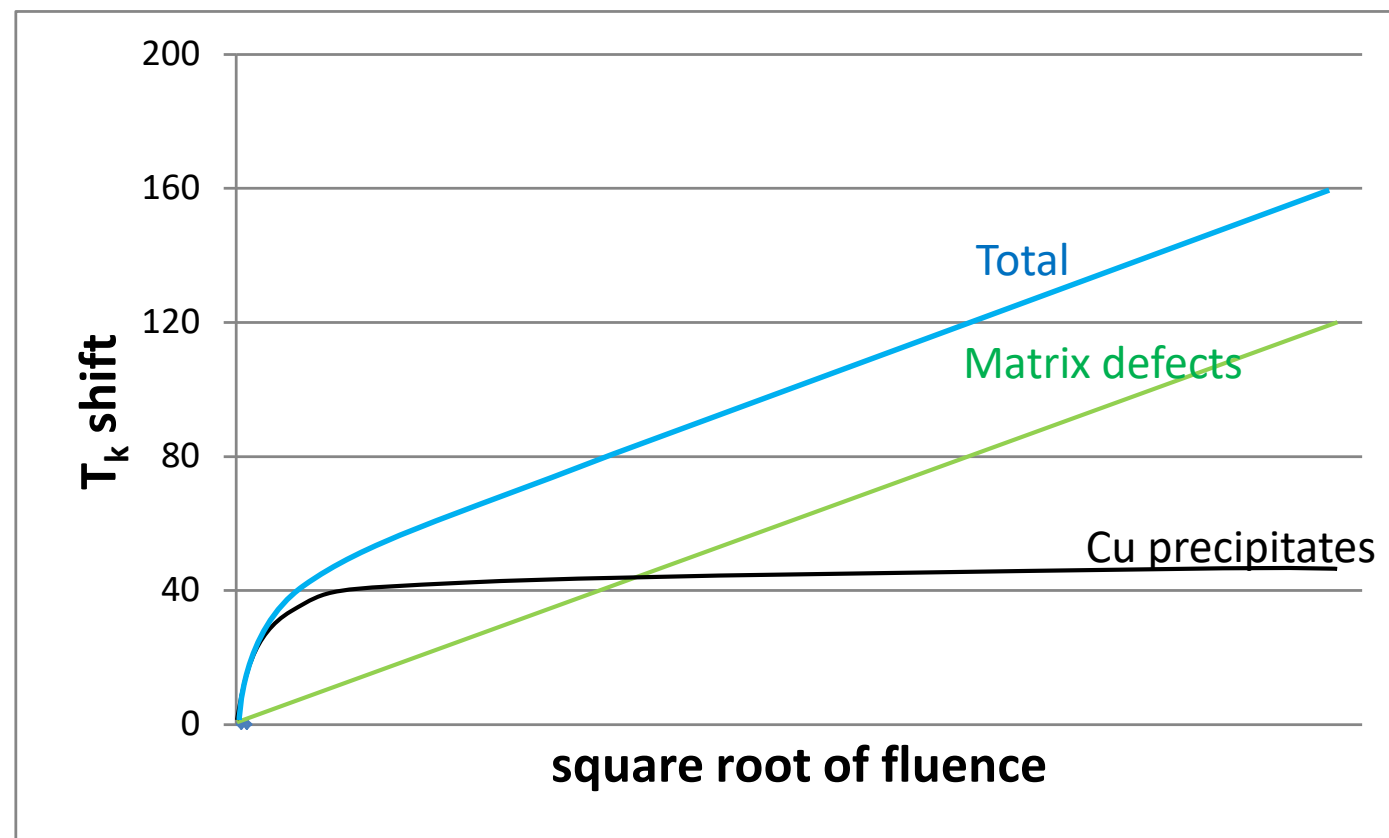
T_k shift recovery due to “wet” annealing - matrix defect elimination



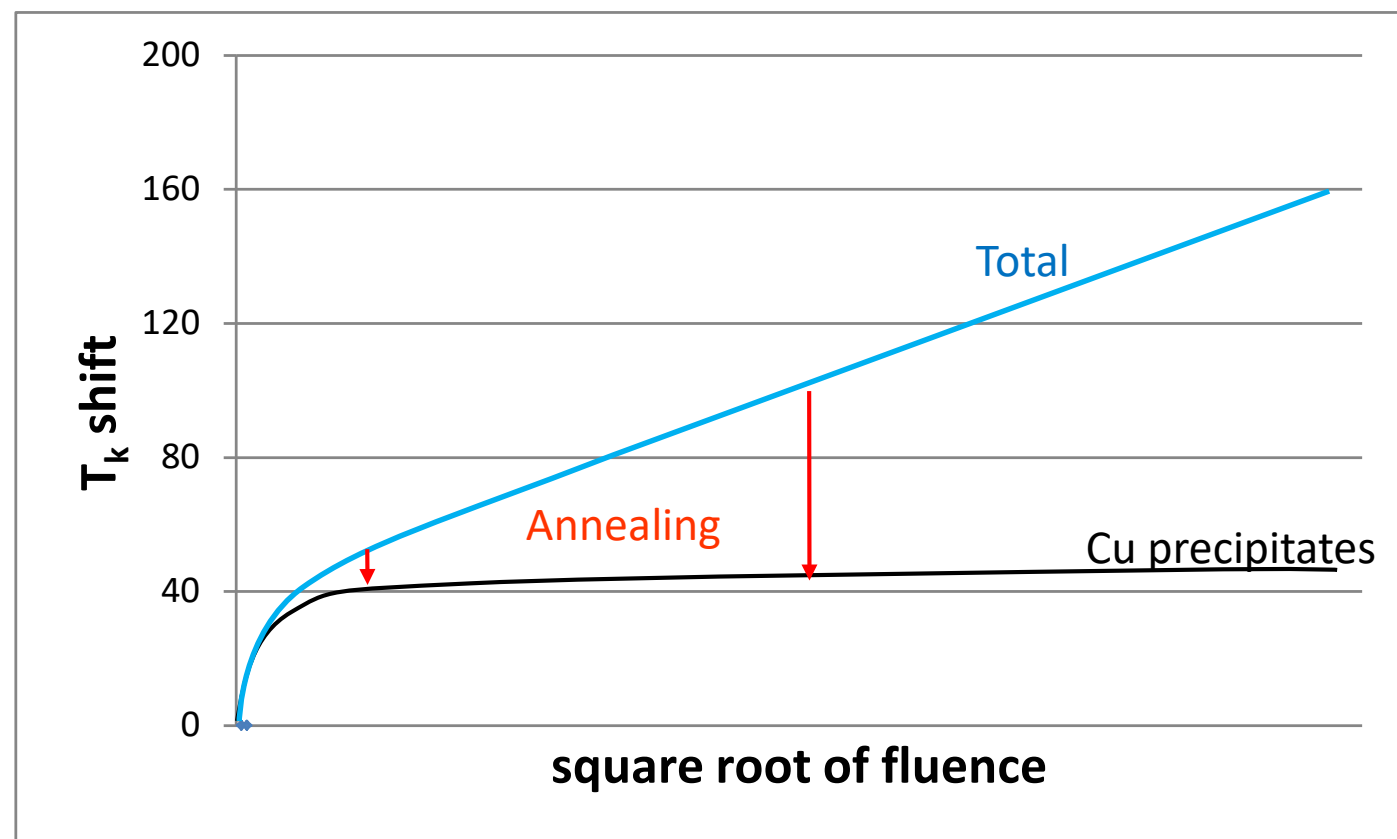
T_k shift recovery due to “wet” annealing - matrix defect elimination



T_k shift recovery due to “wet” annealing - matrix defect elimination

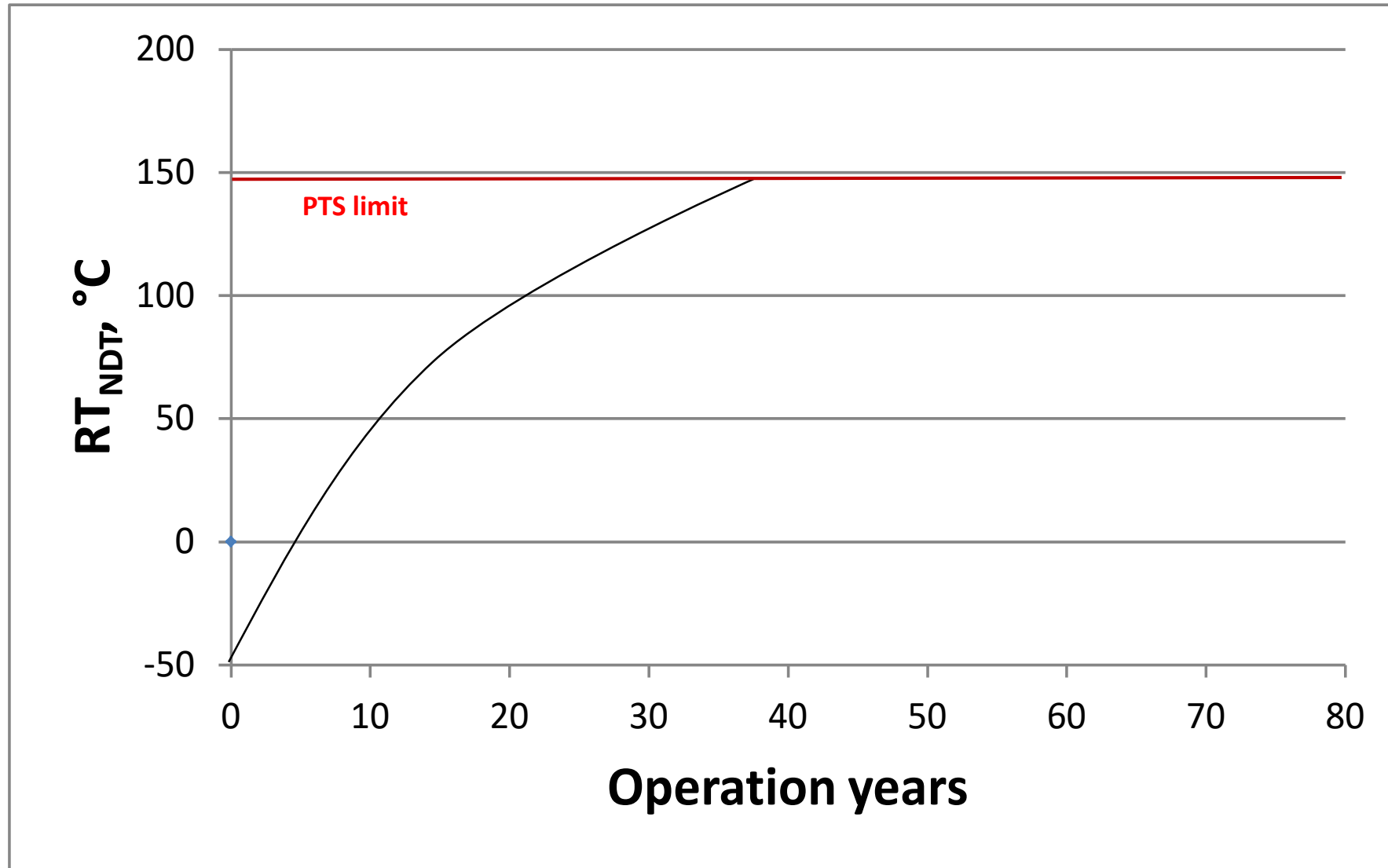


T_k shift recovery due to “wet” annealing - matrix defect elimination

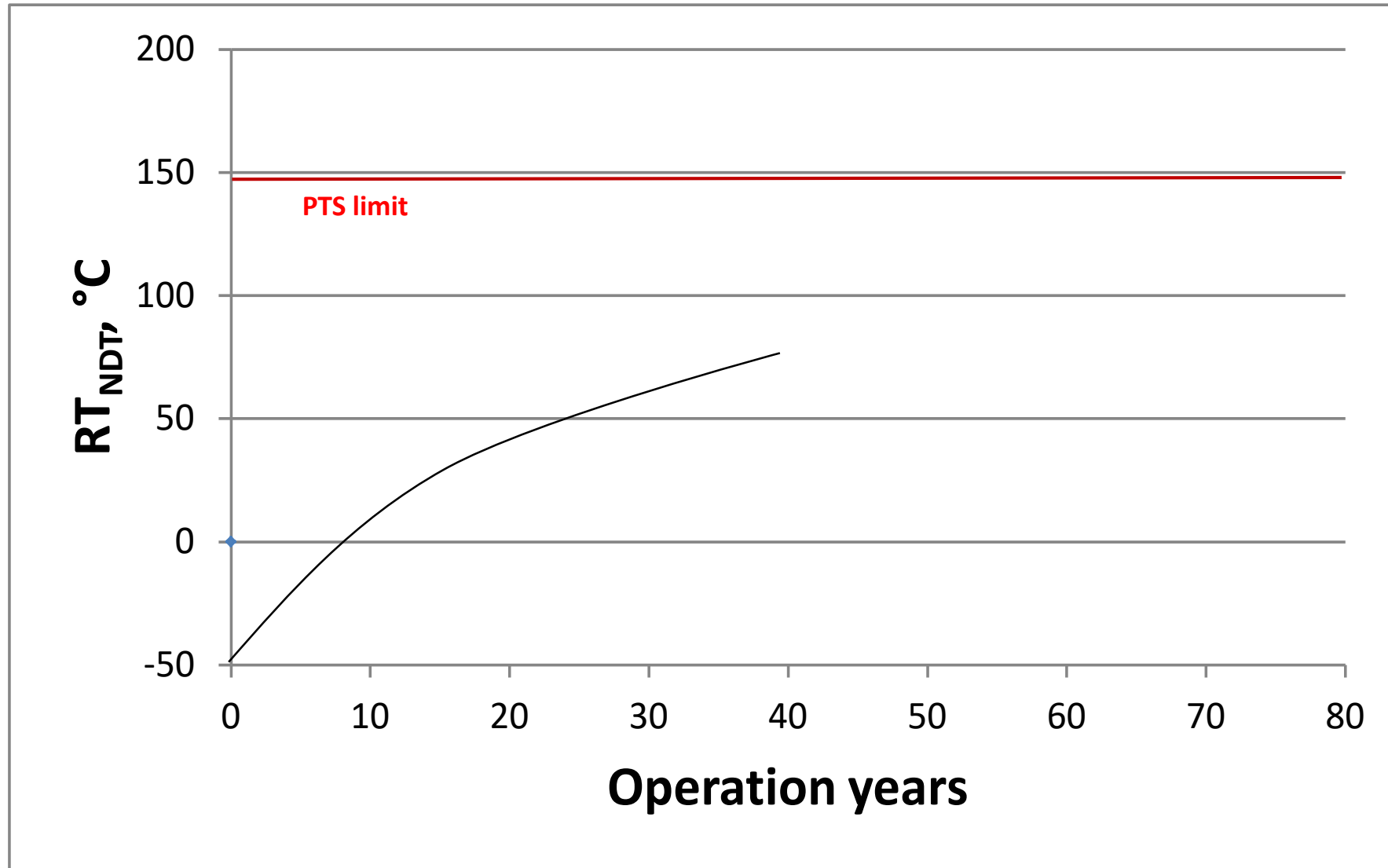


VVER-440 life time long operation

RPV irradiation embrittlement



RPV irradiation embrittlement



VVER RPV-440 life time long term operation



1960s

VVER-440 RPV design fluence:

- $2,4 \cdot 10^{20} \text{ cm}^{-2}$ for base metal
- $1,8 \cdot 10^{20} \text{ cm}^{-2}$ for weld

VVER RPV-440 life time long term operation



1960s

VVER-440 RPV design fluence:

- $2,4 \cdot 10^{20} \text{ cm}^{-2}$ for base metal
- $1,8 \cdot 10^{20} \text{ cm}^{-2}$ for weld

1980s

PNAE G-7-002-86, 1989

VVER RPV-440 life time long term operation



1960s

VVER-440 RPV design fluence:

- $2,4 \cdot 10^{20} \text{ cm}^{-2}$ for base metal
- $1,8 \cdot 10^{20} \text{ cm}^{-2}$ for weld

1980s

PNAE G-7-002-86, 1989

Now

MT 1.2.1.15.0232-2014, Guideline for calculation of brittle fracture resistance of VVER-440 RPV:

Fluence is less $3 \times 10^{20} \text{ cm}^{-2}$

VVER RPV-440 life time long term operation



1960s

VVER-440 RPV design fluence:

$2,4 \cdot 10^{20} \text{ cm}^{-2}$ for base metal

$1,8 \cdot 10^{20} \text{ cm}^{-2}$ for weld

1980s

PNAE G-7-002-86, 1989

Now

MT 1.2.1.15.0232-2014, Guideline for calculation of brittle fracture resistance of VVER-440 RPV:

Fluence is less $3 \times 10^{20} \text{ cm}^{-2}$

Modern requirement – lifetime 60-80 years

VVER RPV-440 life time long term operation



1960s

VVER-440 RPV design fluence:

$2,4 \cdot 10^{20} \text{ cm}^{-2}$ for base metal

$1,8 \cdot 10^{20} \text{ cm}^{-2}$ for weld

1980s

PNAE G-7-002-86, 1989

Now

MT 1.2.1.15.0232-2014, Guideline for calculation of brittle fracture resistance of VVER-440 RPV:

Fluence is less $3 \times 10^{20} \text{ cm}^{-2}$

Modern requirement – lifetime 60-80 years

Options:

- Thermal annealing

VVER RPV-440 life time long term operation



1960s

VVER-440 RPV design fluence:

$2,4 \cdot 10^{20} \text{ cm}^{-2}$ for base metal

$1,8 \cdot 10^{20} \text{ cm}^{-2}$ for weld

1980s

PNAE G-7-002-86, 1989

Now

MT 1.2.1.15.0232-2014, Guideline for calculation of brittle fracture resistance of VVER-440 RPV:

Fluence is less $3 \times 10^{20} \text{ cm}^{-2}$

Modern requirement – lifetime 60-80 years

Options:

- Thermal annealing
- Validation of T_k vs fluence dependences for fluence more $3 \times 10^{20} \text{ cm}^{-2}$

Objective – VVER-440 RPV integrity validation
at neutron fluence up to $5 \times 10^{20} \text{ cm}^{-2}$ (~ 80 years operation)

The highest contents of impurities and fluence values both in the worldwide used RPV steels and in the **IAEA Database**



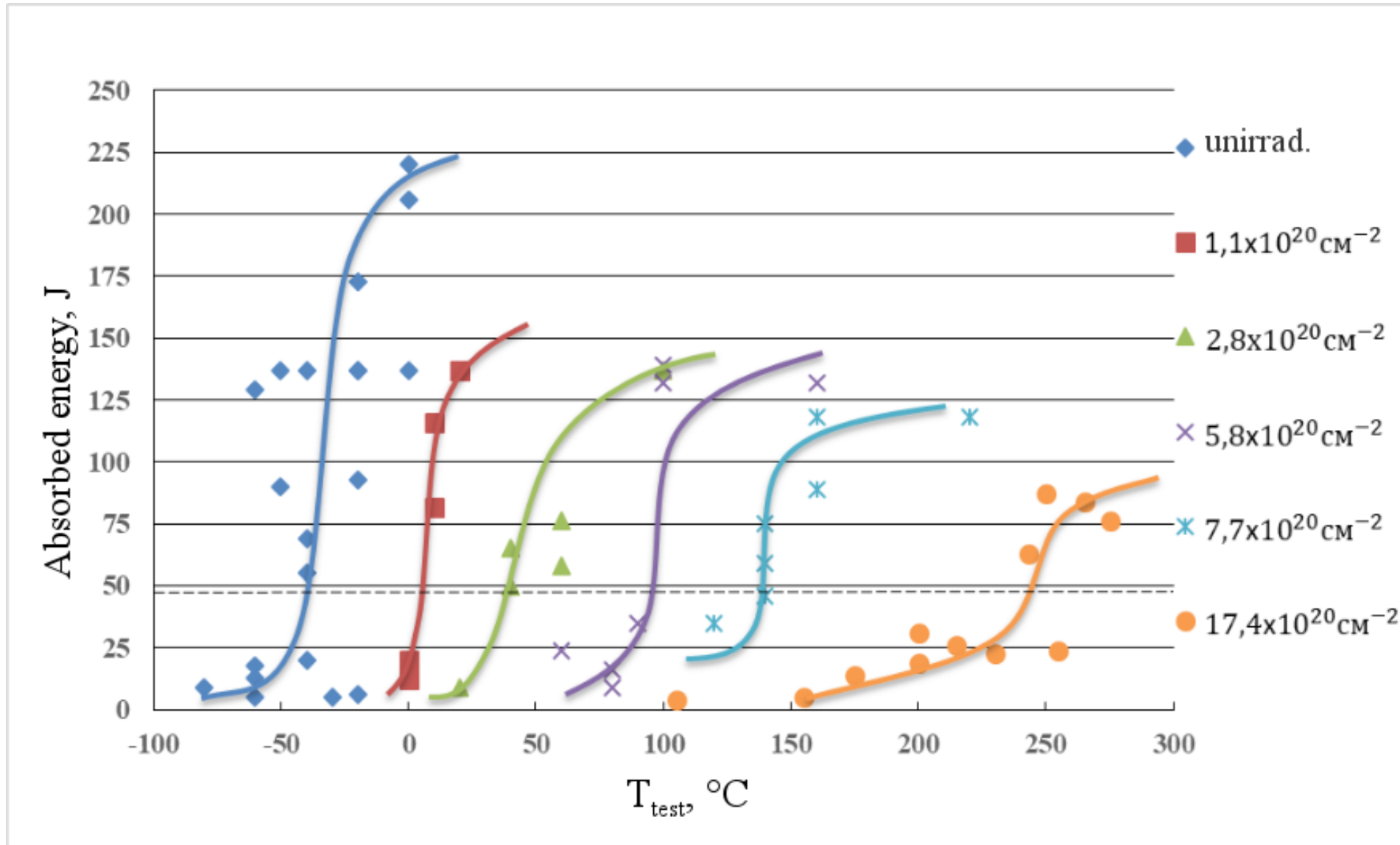
Reactor type	Cu_{max}, wt %	P_{max}, wt %	Ni_{max}, wt %	Mn_{max}, wt %	Fluence_{max}, n/cm²
PWR	0.42	0.025	1.2	2.1	3.7 x 10¹⁹, E>1 MeV
VVER	0.20	0.042	1.9	1.3	2.4 x 10²⁰, E>0.5 MeV
Surveillance data	0.35	0.035	1.9	2.1	~15 x 10²⁰, E>0.5 MeV
Research programme data	0.4	0.045	2.8	2.0	~20 x 10²⁰, E>0.5 MeV

IAEA database for VVER-440 RPV surveillance test results



№	Country	NPP	Unit
1	Armenia	Mezhamor	2
2	Russia	Kola	3
3	Russia	Kola	4
4	Ukraine	Rovno	1
5	Ukraine	Rovno	2
6	Hungary	Paks	1
7	Hungary	Paks	2
8	Hungary	Paks	3
9	Hungary	Paks	4
10	Slovak Republic	Bohunice	3
11	Slovak Republic	Bohunice	4
12	Czech Republic	Dukovany	1
13	Czech Republic	Dukovany	2
14	Czech Republic	Dukovany	3
15	Czech Republic	Dukovany	4

Rovno 2 base metal surveillance results



Analysis of highly irradiated surveillance specimens results

Group of steels	Phosphorus content	Cupper content
"Clean"	$P \leq 0,012\%$,	$Cu \leq 0,07\%$

Analysis of highly irradiated surveillance specimens results

Group of steels	Phosphorus content	Cupper content
“Clean”	$P \leq 0,012\%$,	$Cu \leq 0,07\%$
Almost “clean”	$0,017\% \geq P \geq 0,012\%$,	$0,14\% \geq Cu \geq 0,07\%$

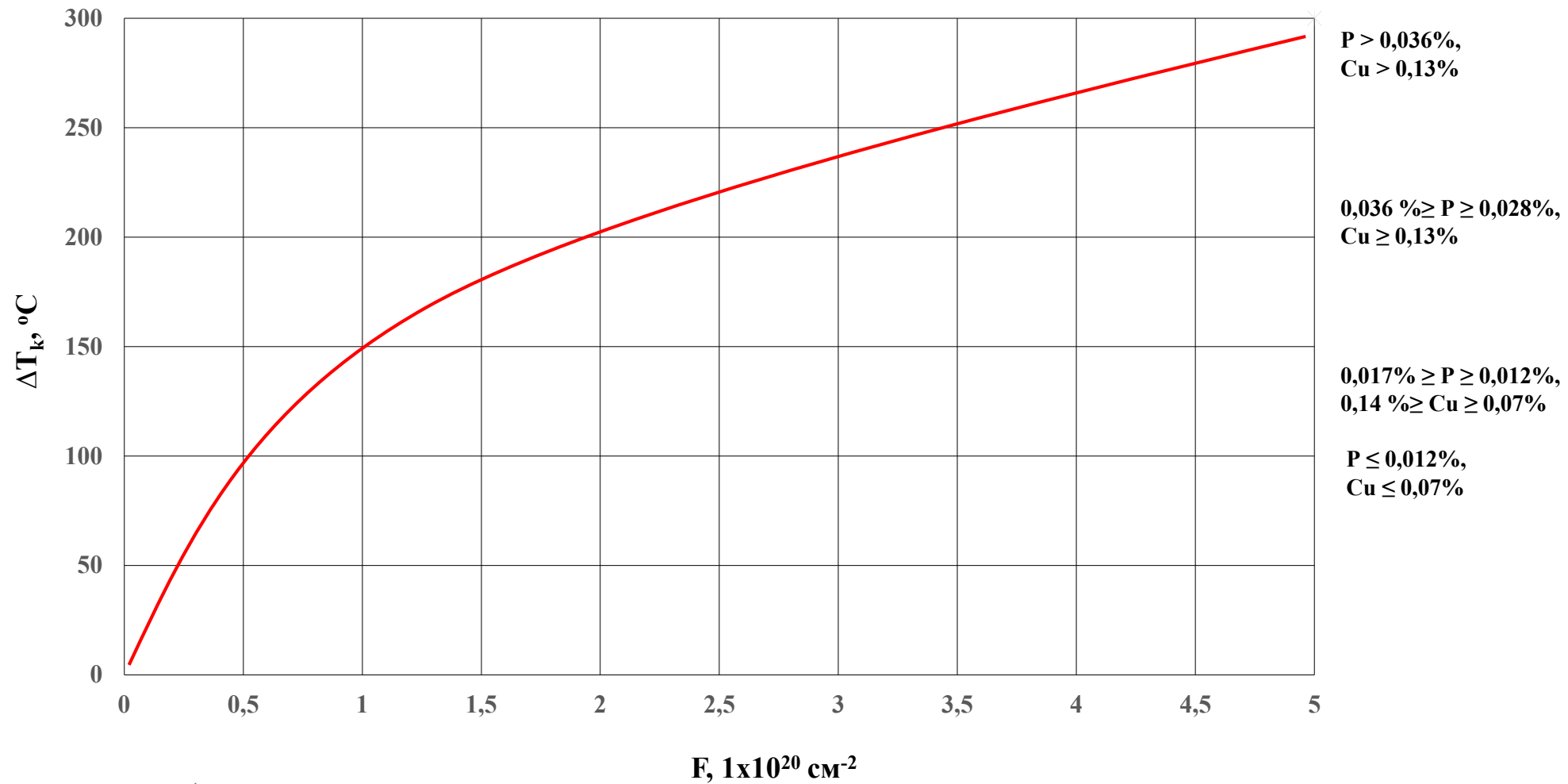
Analysis of highly irradiated surveillance specimens results

Group of steels	Phosphorus content	Copper content
“Clean”	$P \leq 0,012\%$,	$Cu \leq 0,07\%$
Almost “clean”	$0,017\% \geq P \geq 0,012\%$,	$0,14\% \geq Cu \geq 0,07\%$
“Dirty”	$0,036\% \geq P \geq 0,028\%$,	$Cu \geq 0,13\%$

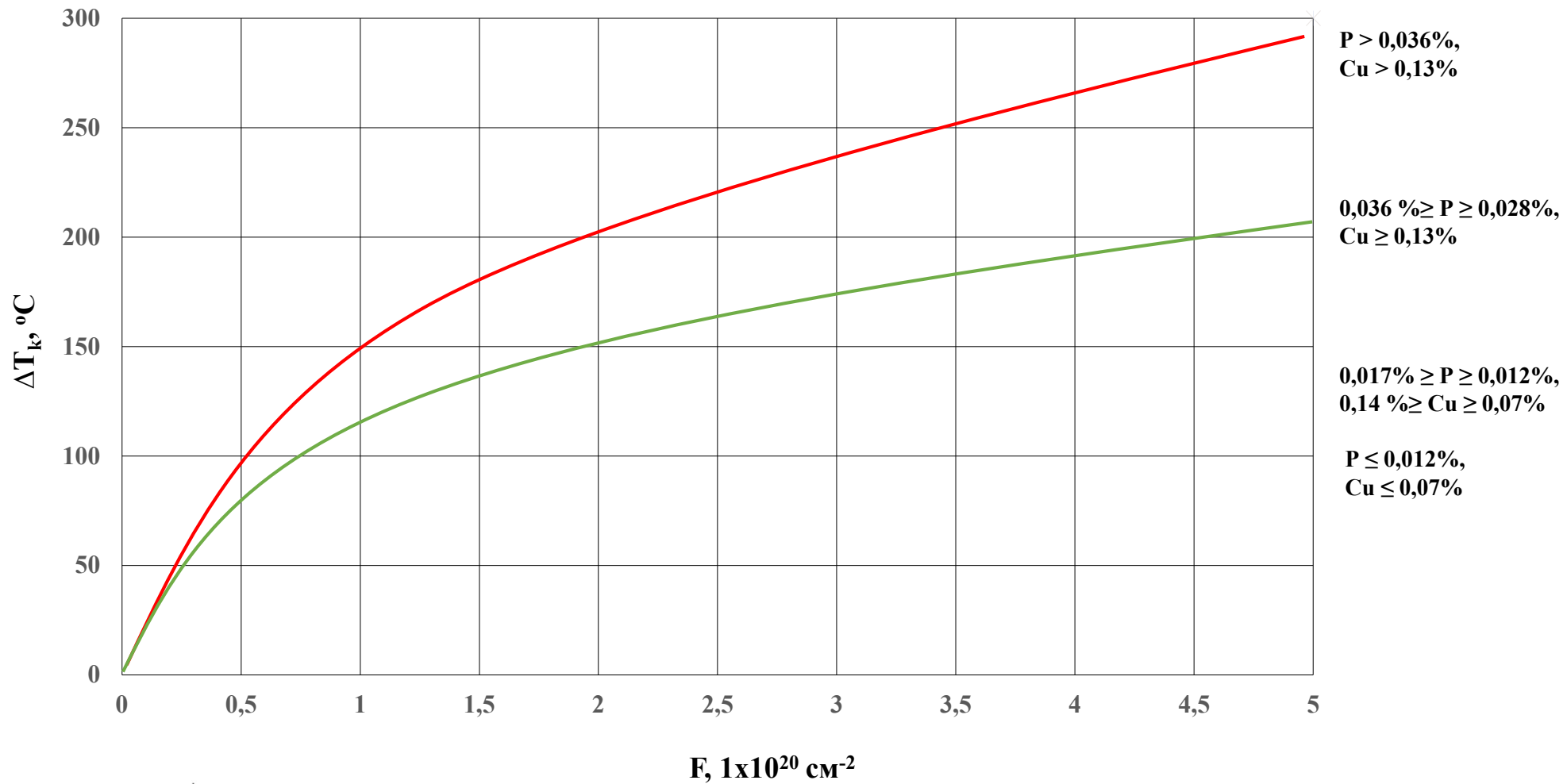
Analysis of highly irradiated surveillance specimens results

Group of steels	Phosphorus content	Copper content
“Clean”	$P \leq 0,012\%$,	$Cu \leq 0,07\%$
Almost “clean”	$0,017\% \geq P \geq 0,012\%$,	$0,14\% \geq Cu \geq 0,07\%$
“Dirty”	$0,036\% \geq P \geq 0,028\%$,	$Cu \geq 0,13\%$
Highly “dirty”	$P > 0,036\%$,	$Cu > 0,13\%$

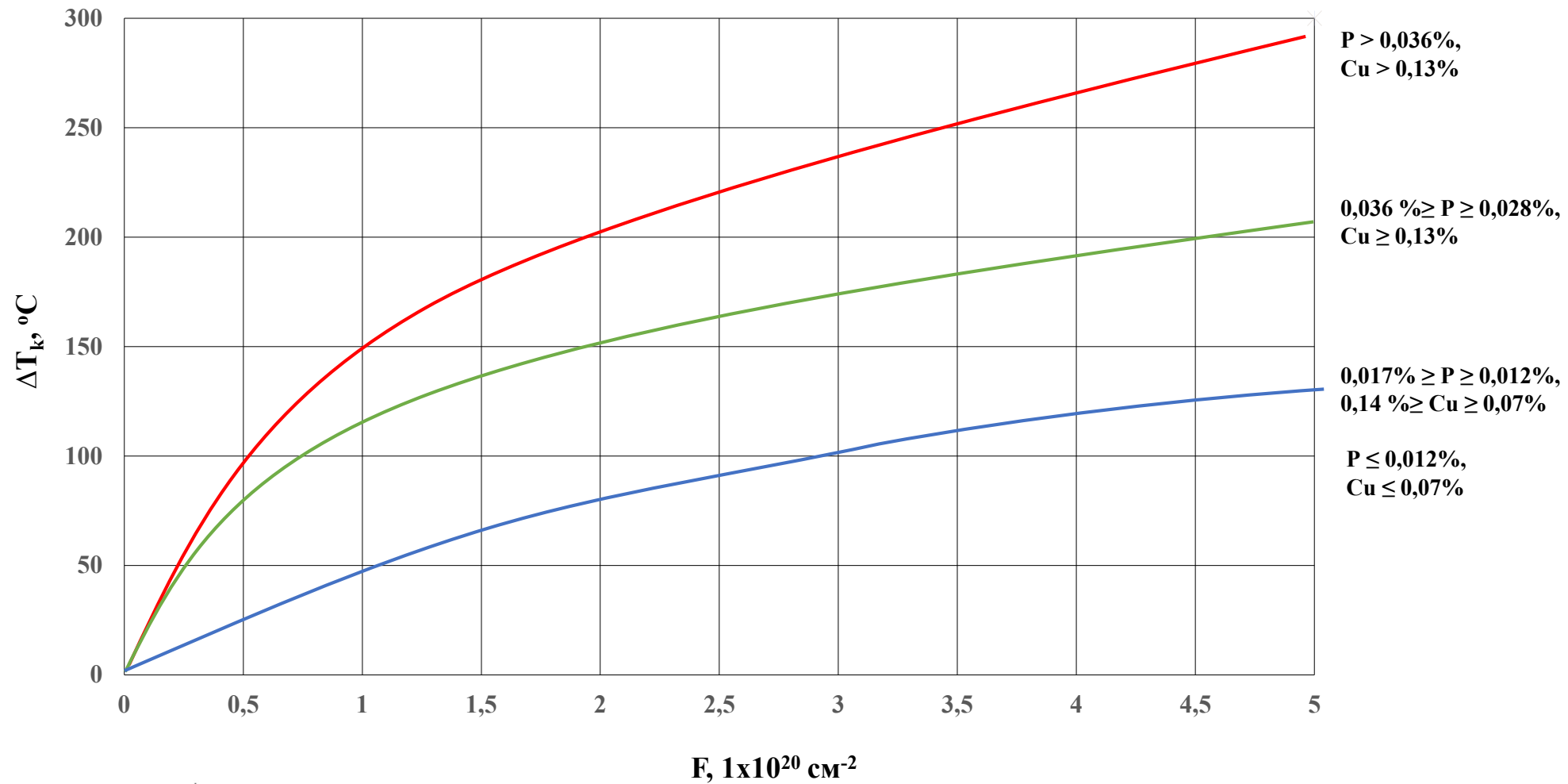
Irradiation embrittlement of VVER-440 RPV steels



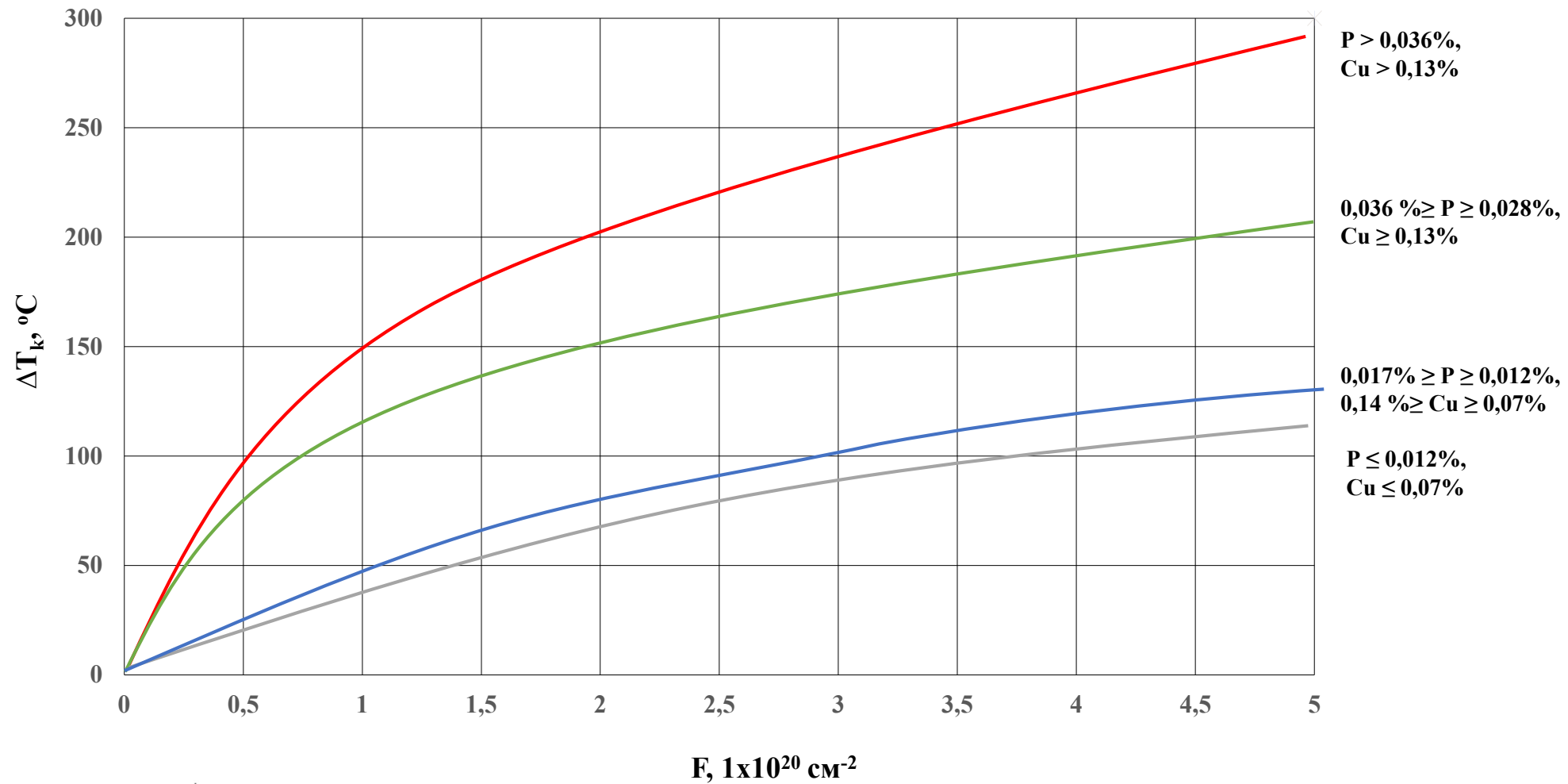
Irradiation embrittlement of VVER-440 RPV steels



Irradiation embrittlement of VVER-440 RPV steels



Irradiation embrittlement of VVER-440 RPV steels



Results of highly irradiated surveillance data analysis

- T_K shift is not more 100 -130 °C for low Cu и P steels

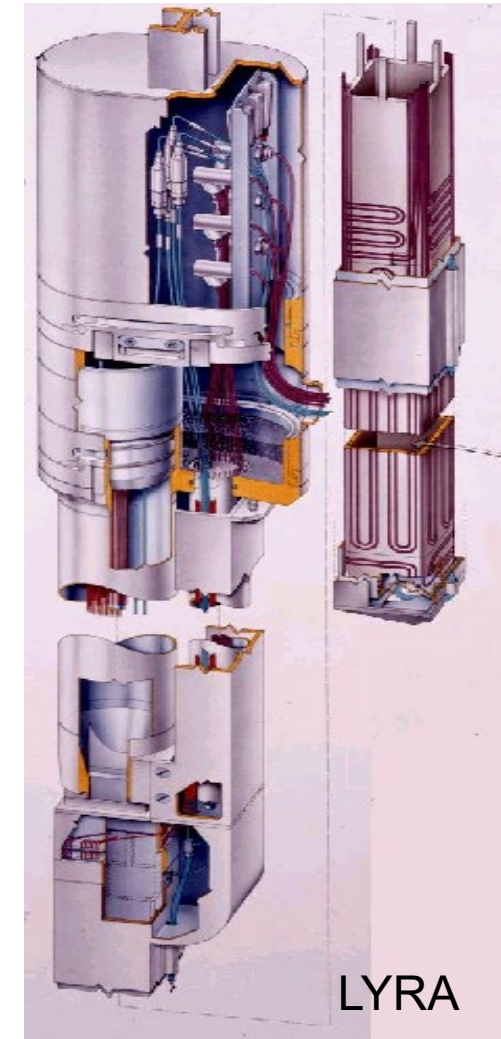
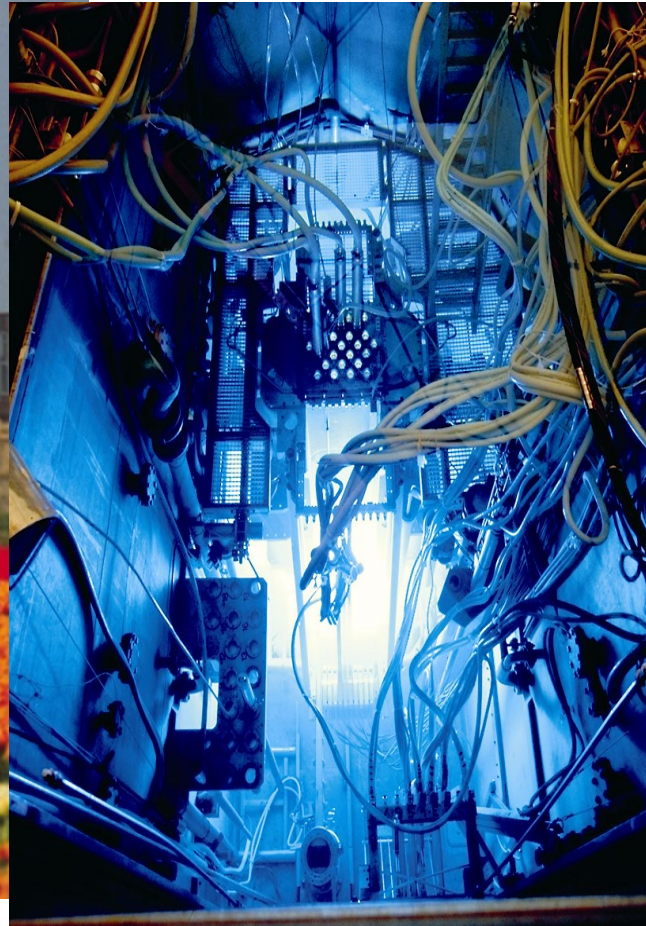
Results of highly irradiated surveillance data analysis

- T_K shift is not more 100 -130 °C for low Cu и P steels
- Lifetime of VVER-440 RPV could be validated up to fluence $5 \times 10^{20} \text{ cm}^{-2}$ (~ 80 years operation) without thermal annealing

STRUMAT

(**STR**Uctural **MA**TeriAls research for safe Long Term Operation of LWR NPPs)

Joined JRC – NRG project irradiation in HFR, Petten



Project aim – validation of irradiation embrittlement assessment for RPV **long term operation**



**Project aim – validation of irradiation embrittlement assessment
for RPV **long term operation****



Key point: establishment of **synergistic interactions between Ni and Mn
for low Cu RPV steels at high fluence**

Project aim – validation of irradiation embrittlement assessment for RPV **long term operation**



**Key point: establishment of synergistic interactions between Ni and Mn
for low Cu RPV steels at high fluence**

- Conclusion of “IAEA High Ni” CRP, 2000-2004

Project aim – validation of irradiation embrittlement assessment for RPV **long term operation**



**Key point: establishment of synergistic interactions between Ni and Mn
for low Cu RPV steels at high fluence**

- Conclusion of “IAEA High Ni” CRP, 2000-2004
- **12 model steels and 8 submerged arc welds**

Project aim – validation of irradiation embrittlement assessment for RPV **long term operation**



**Key point: establishment of synergistic interactions between Ni and Mn
for low Cu RPV steels at high fluence**

- Conclusion of “IAEA High Ni” CRP, 2000-2004
- **12 model steels and 8 submerged arc welds**
- Ni and Mn variations cover the range between minimum and maximum found in PWR and VVER

Project aim – validation of irradiation embrittlement assessment for RPV **long term operation**



**Key point: establishment of synergistic interactions between Ni and Mn
for low Cu RPV steels at high fluence**

- Conclusion of “IAEA High Ni” CRP, 2000-2004
- **12 model steels and 8 submerged arc welds**
- Ni and Mn variations cover the range between minimum and maximum found in PWR and VVER
- Target fluence $6 \times 10^{19} \text{ cm}^{-2}$ (60-80 years of PWR operation)

Project aim – validation of irradiation embrittlement assessment for RPV **long term operation**

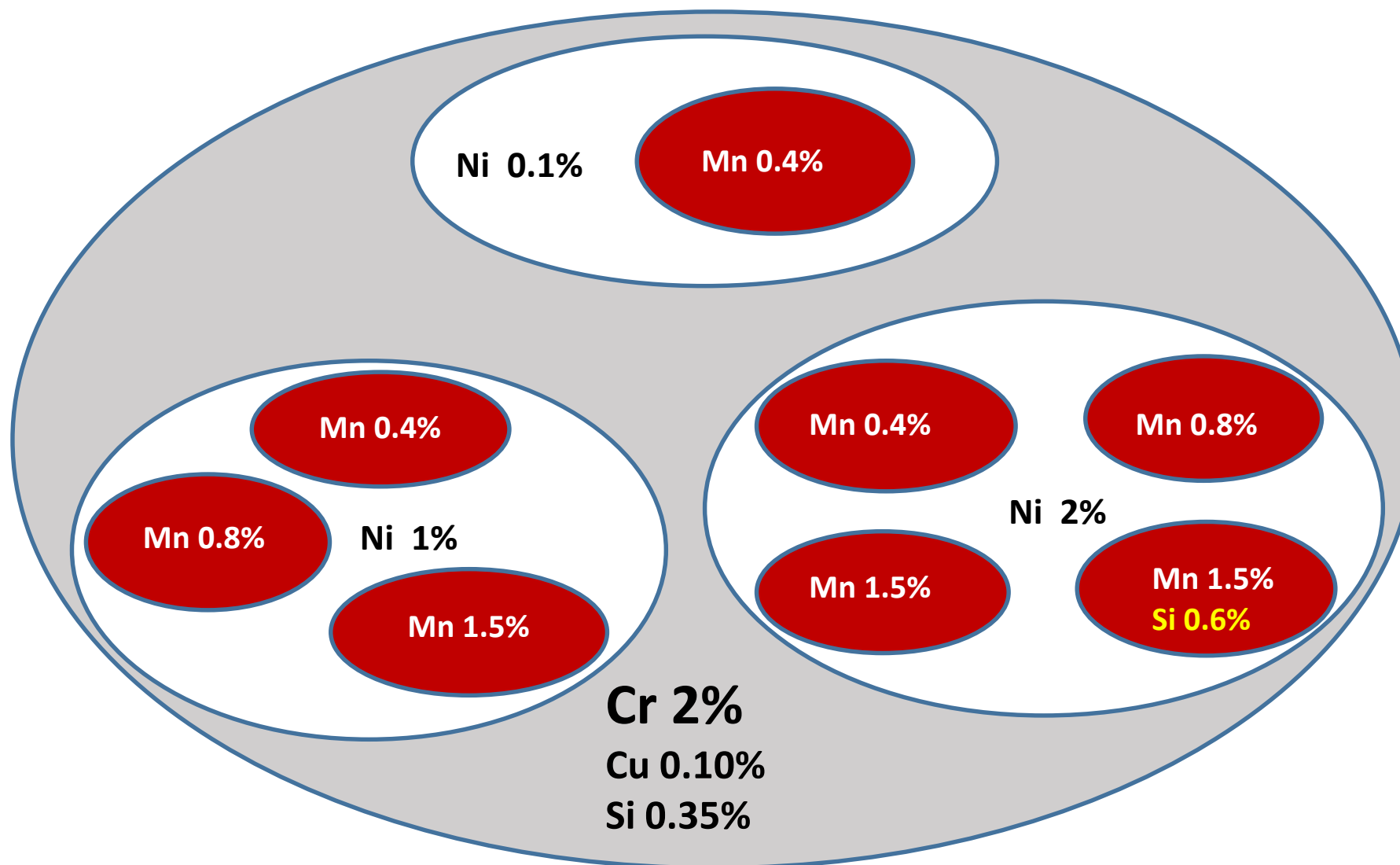


**Key point: establishment of synergistic interactions between Ni and Mn
for low Cu RPV steels at high fluence**

- Conclusion of “IAEA High Ni” CRP, 2000-2004
- **12 model steels and 8 submerged arc welds**
- Ni and Mn variations cover the range between minimum and maximum found in PWR and VVER
- Target fluence $6 \times 10^{19} \text{ cm}^{-2}$ (60-80 years of PWR operation)
- Irradiation in HFR finished in January 2018

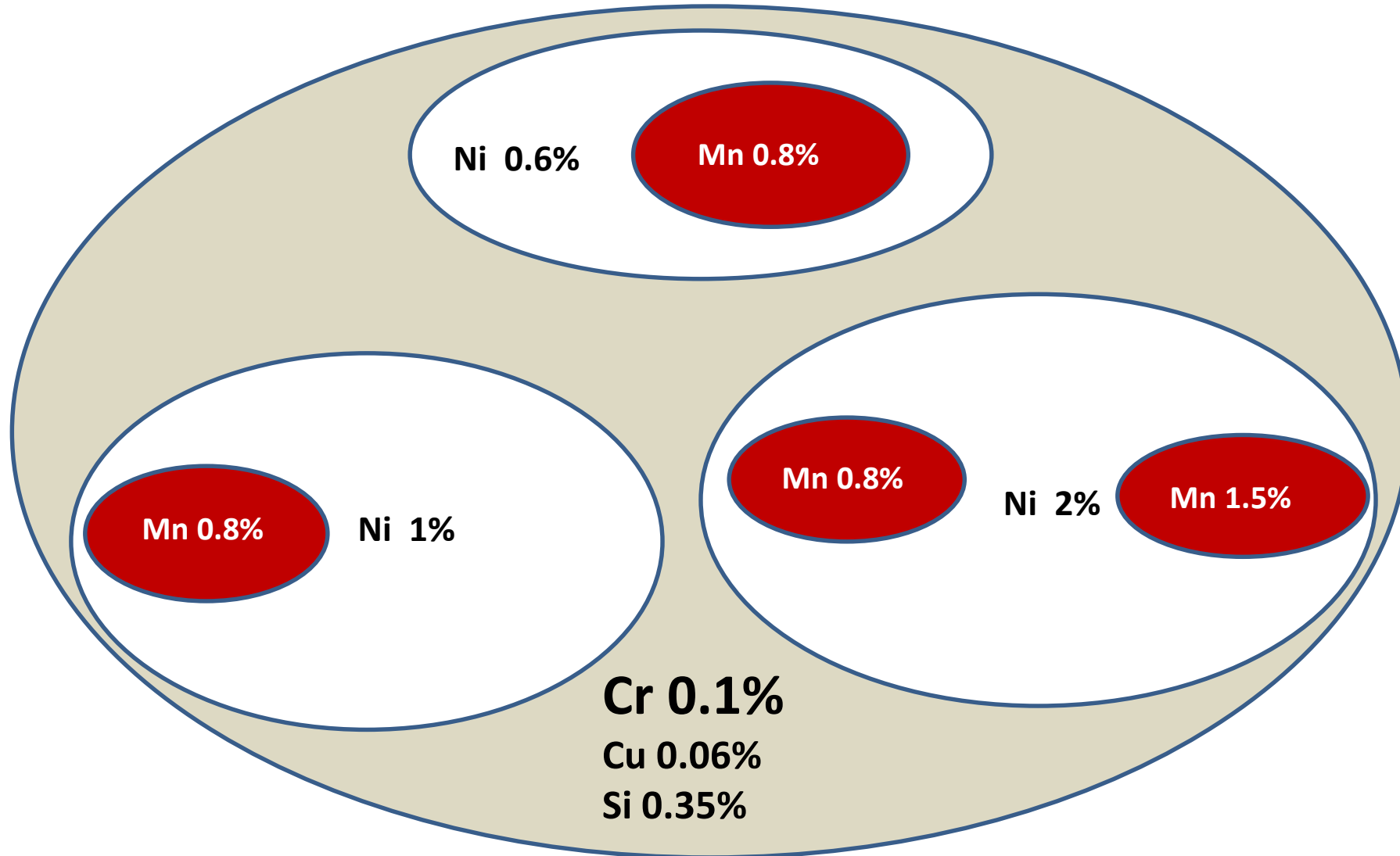
8 model steels

Ni & Mn variations in VVER RPVs



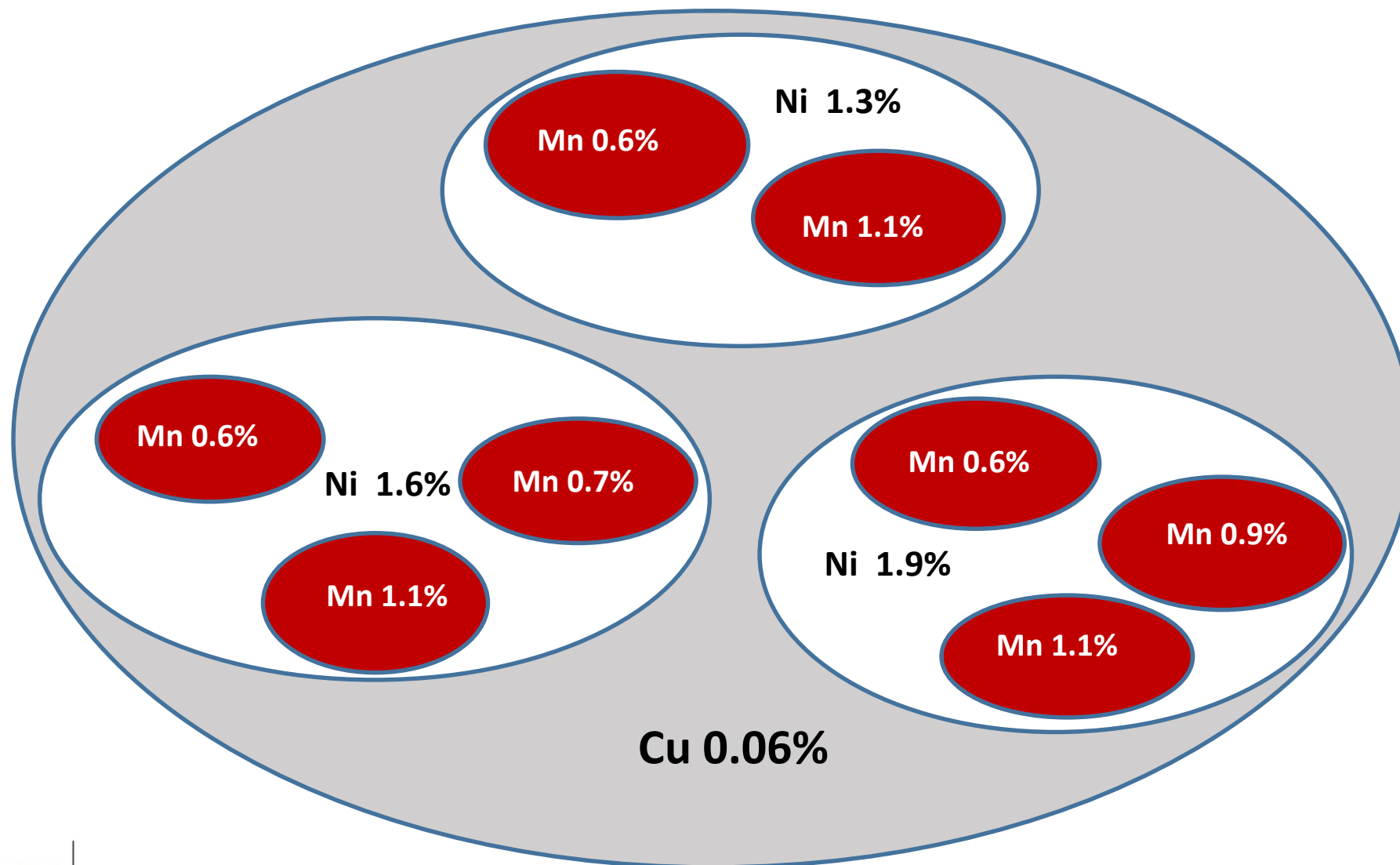
4 model steels

Ni & Mn variations in PWR RPVs



8 submerged arc welds

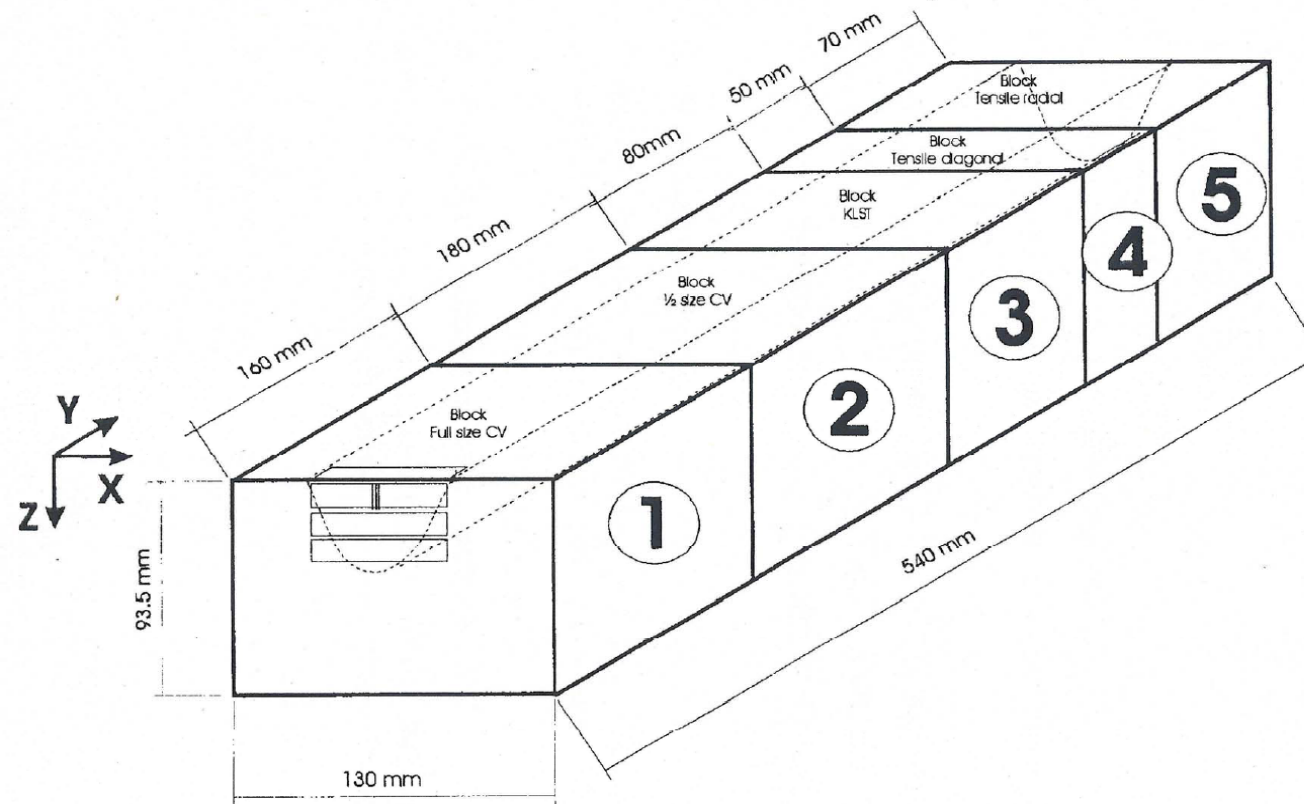
Ni & Mn variations in low Cu RPV welds



8 Low Cu high Ni&Mn submerged arc welds



- Skoda Plzen plant in Czech Republic
- 8 single V-preparation submerged arc welds in **190 mm thick plate**



KLST and tensile specimens, Charpy (4 welds),
slices 6x10x0.5 mm for microstructural examination

Project participants

Research centres:

- EC JRC (EU)
- NRG (The Netherlands)
- HZDR (Germany)
- VTT (Finland)
- Fraunhofer Institute for Nondestructive Testing (Germany)
- CIEMAT (Spain)
- UJV Rzez (Czech Republic)
- Hungarian Academy of Science Centre for Energy Research (Hungary)
- Bay Zoltan Nonprofit Ltd (Hungary)
- University of Manchester (UK)
- Kiev Institute for Nuclear Research (Ukraine)
- VUJE (Slovakia)
- Slovak University (Slovakia)

Regulators:

- STUK (Finland)
- United Kingdom Atomic Energy Authority
- SEC NRS (Russia)
- Analytical Research Bureau for NPP Safety (Ukraine)

SEC NRS role – scientific support of STRUMAT post irradiation examination

Conclusions

Radiation damage - most important RPV ageing mechanism

Conclusions

Radiation damage - most important RPV ageing mechanism

RPV lifetime controlled by radiation damage of RPV beltline materials

Conclusions

Radiation damage - most important RPV ageing mechanism

RPV lifetime controlled by radiation damage of RPV beltline materials

Irradiation embrittlement together with material initial properties determines RPV lifetime

Conclusions

Radiation damage - most important RPV ageing mechanism

RPV lifetime controlled by radiation damage of RPV beltline materials

Irradiation embrittlement together with material initial properties determines RPV lifetime

Thermal annealing – most effective instrument to mitigate irradiation embrittlement

Conclusions

Radiation damage - most important RPV ageing mechanism

RPV lifetime controlled by radiation damage of RPV beltline materials

Irradiation embrittlement together with material initial properties determines RPV lifetime

Thermal annealing – most effective instrument to mitigate irradiation embrittlement

“Wet” annealing is effective for RPV steels with low P & Cu contents

Conclusions

Radiation damage - most important RPV ageing mechanism

RPV lifetime controlled by radiation damage of RPV beltline materials

Irradiation embrittlement together with material initial properties determines RPV lifetime

Thermal annealing – most effective instrument to mitigate irradiation embrittlement

“Wet” annealing is effective for RPV steels with low P & Cu contents

End of lifetime fluence of VVER-440 RPV could be extended up to $5 \times 10^{20} \text{ cm}^{-2}$

Conclusions

Radiation damage - most important RPV ageing mechanism

RPV lifetime controlled by radiation damage of RPV beltline materials

Irradiation embrittlement together with material initial properties determines RPV lifetime

Thermal annealing – most effective instrument to mitigate irradiation embrittlement

“Wet” annealing is effective for RPV steels with low P & Cu contents

End of lifetime fluence of VVER-440 RPV could be extended up to $5 \times 10^{20} \text{ cm}^{-2}$

Basic resented event in ageing mechanism area - STRUMAT project aimed to validation of irradiation embrittlement for RPV long term operation