

Chun-Liang Zhang

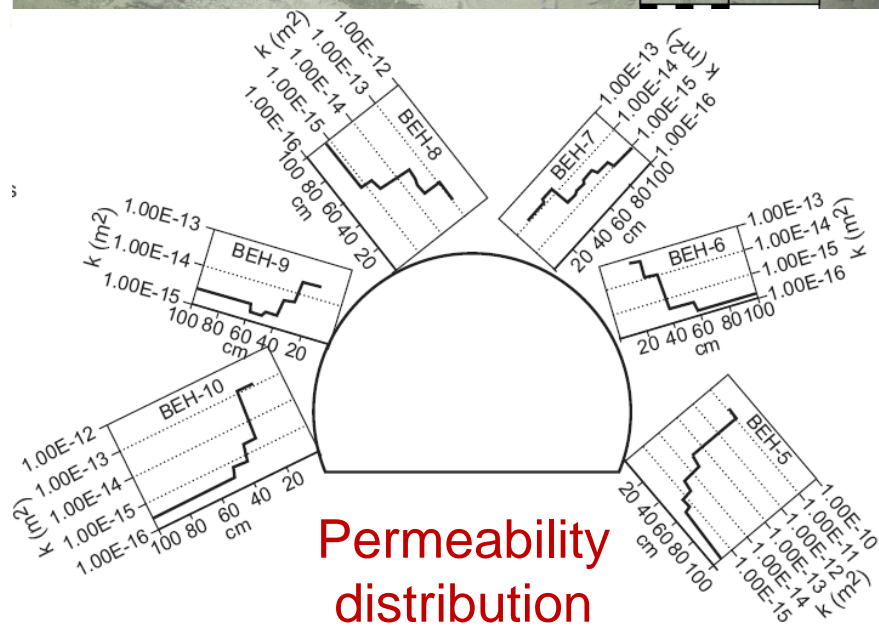
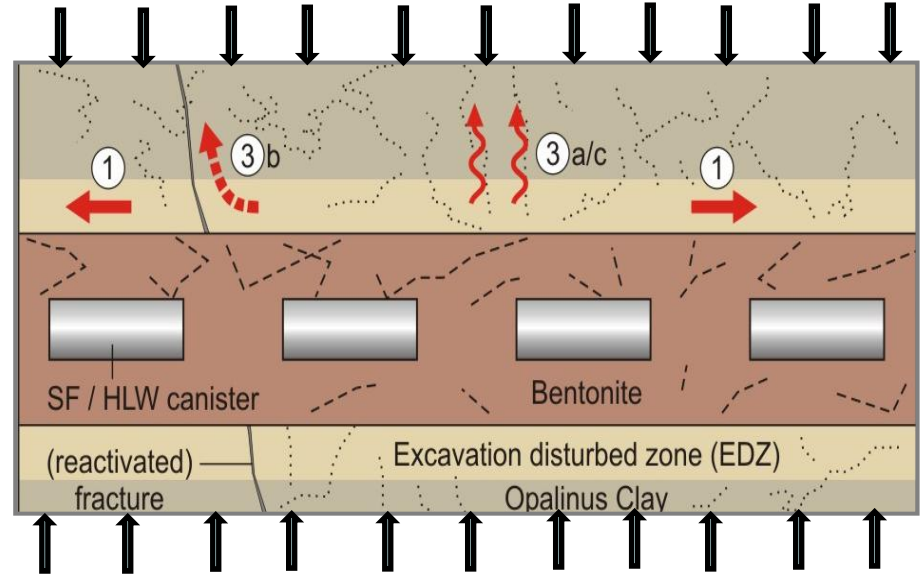
GRS Repository Safety Research Division, Germany

Self-Sealing of Fractures in Clay Rock for Disposal of Radioactive Waste

Excavation Damaged Zone



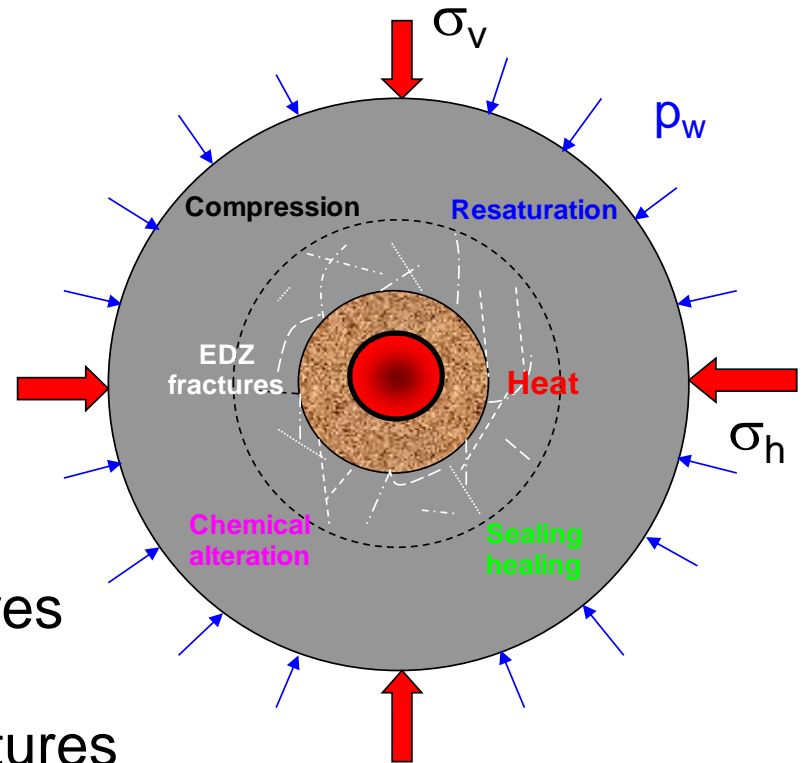
Sealing of EDZ expected



- Rock rheological compression & backfill withstand
- Swelling of claystone in EDZ by water uptake

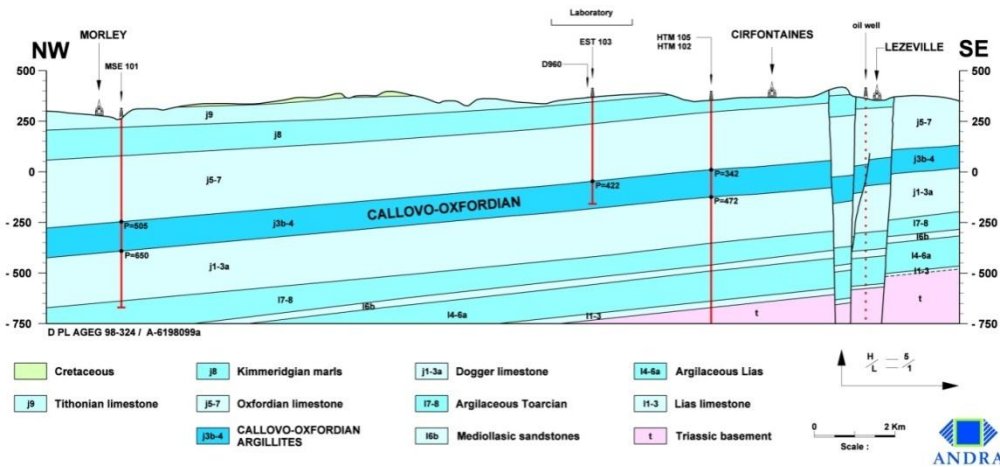
Experimental Evidence for Sealing of Fractures

1. Rock mechanical compression
2. Water-enhanced sealing of fractures
3. Thermal impact on sealing of fractures
4. Simulation of EDZ evolution around boreholes



Clay Rocks investigated at GRS Laboratory

Callovo-Oxfordian Argillite at the URL Bure

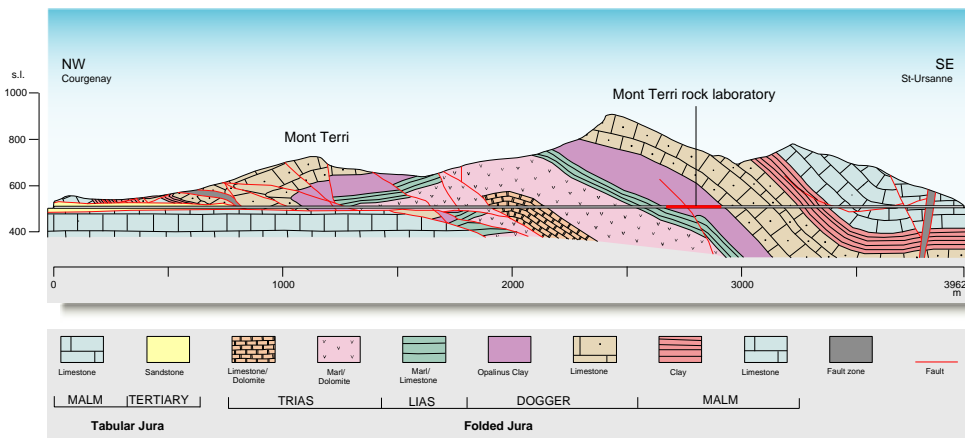


D28cm, L52cm

Basic characters

clay content	~42 %
water content	7.7 %
porosity	13~17 %
permeability	$< 10^{-20} \text{ m}^2$
uniaxial strength	20~30 MPa

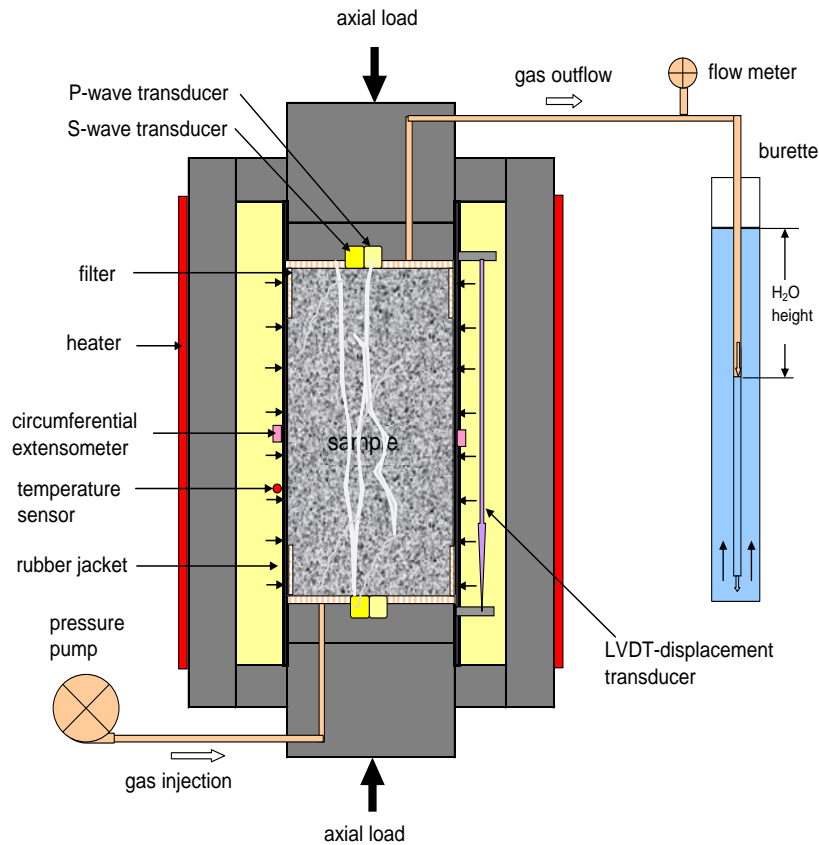
Opalinus Clay at the URL Mont Terri



D28cm, L70cm

clay content	~65 %
water content	6.7 %
porosity	14~17 %
permeability	$< 10^{-20} \text{ m}^2$
uniaxial strength	10~15 MPa

1. Sealing of fractures under mechanical compression



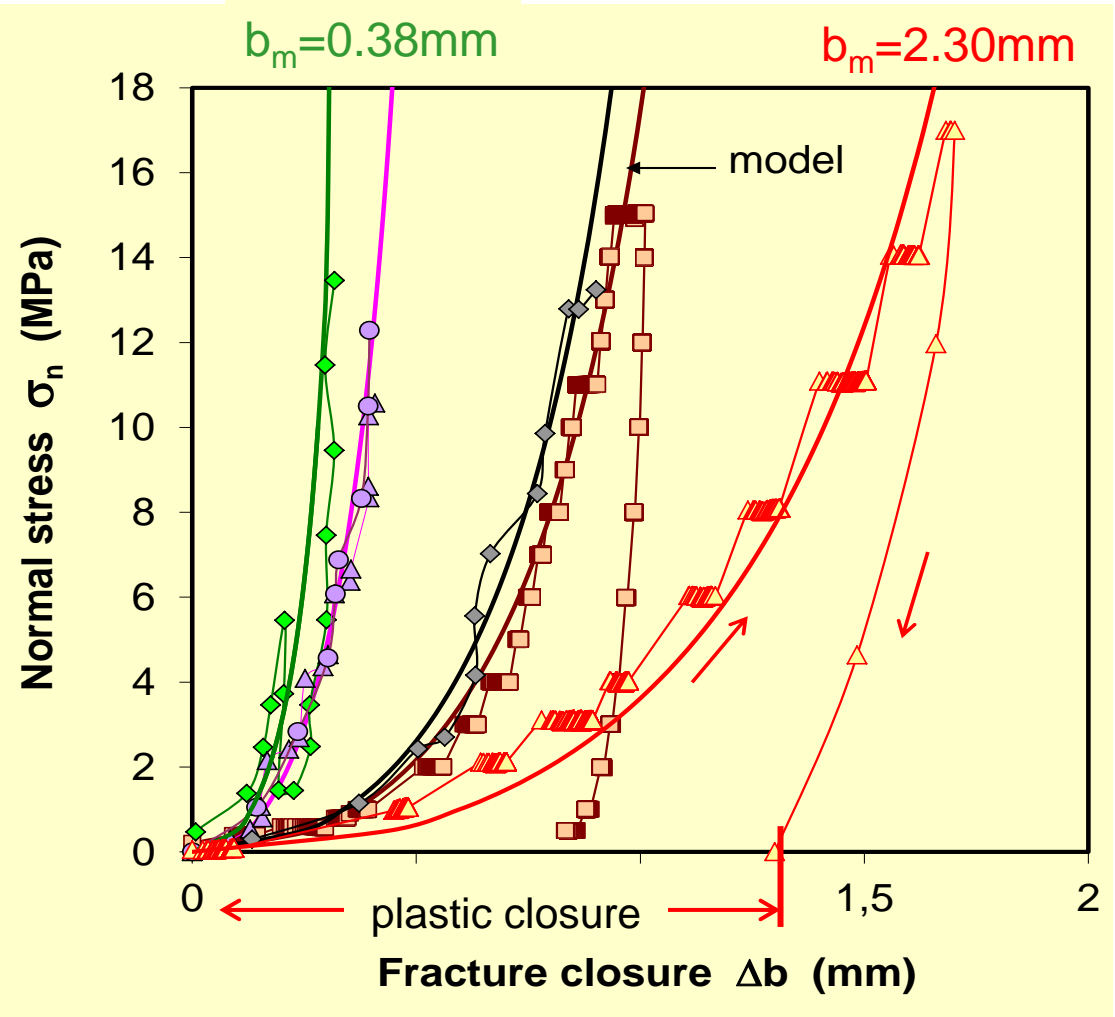
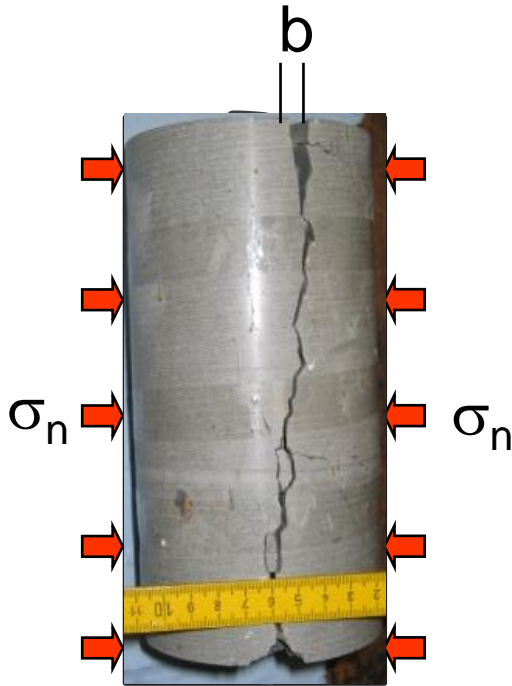
COX sample



OPA sample

fracture closure
gas permeability

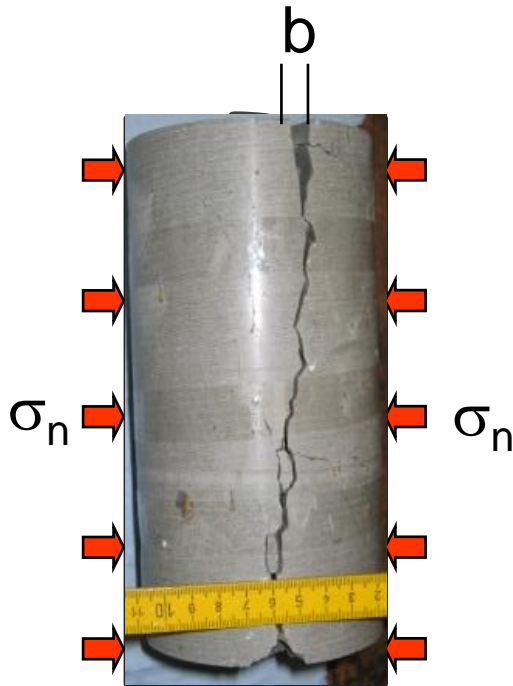
Fracture closure under normal stress



$$\Delta b = b_m \left[1 - \exp\left(-\alpha \sigma_n^\beta\right) \right]$$

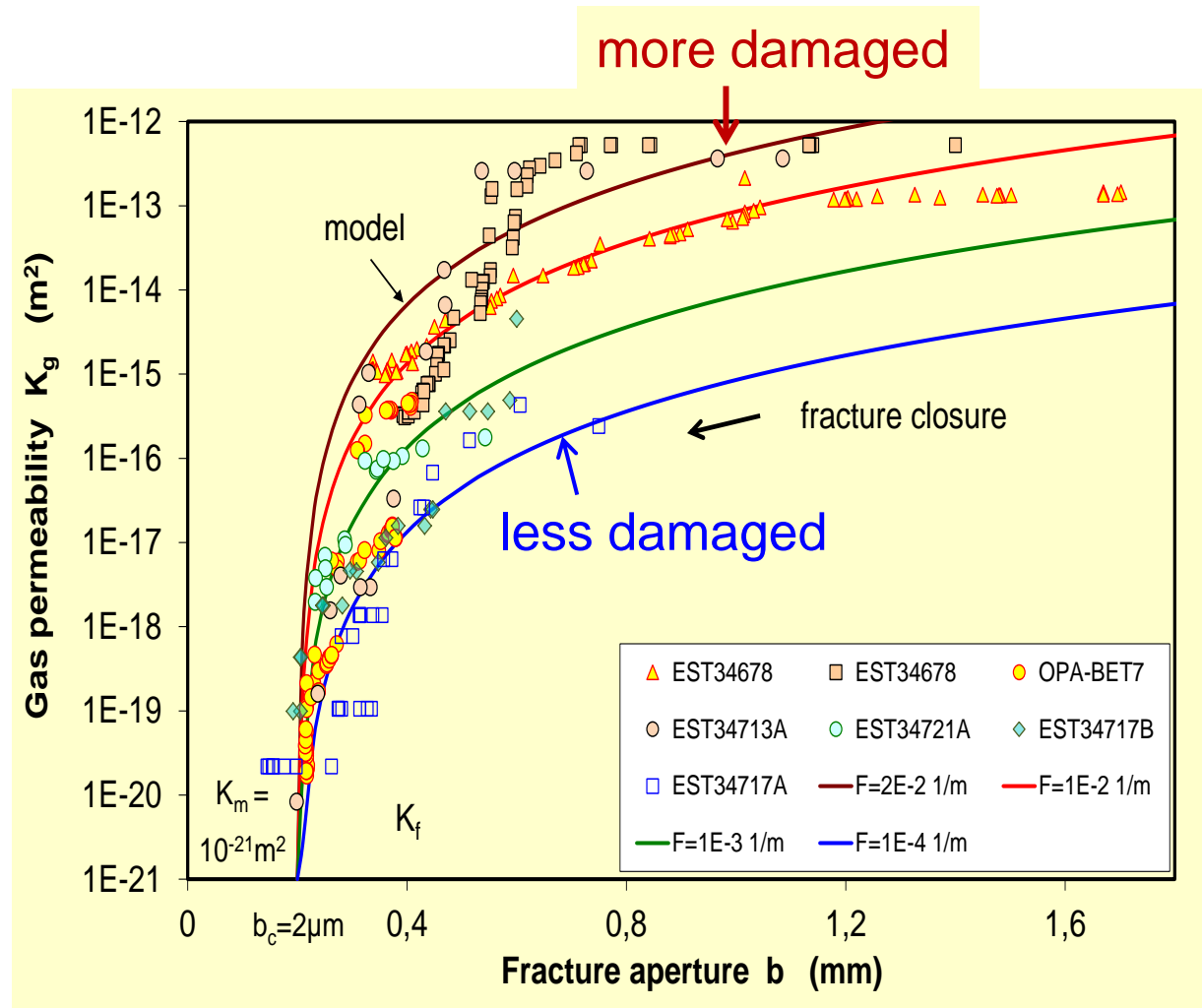
$$\sigma_n \rightarrow \infty \implies b \rightarrow 0$$

Fracture closure and permeability decrease

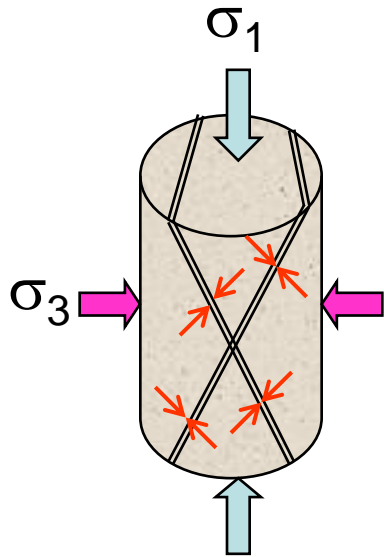


$$K = K_m + \frac{R(b - b_c)^3}{12s}$$

$$b \rightarrow b_c \implies K \rightarrow K_m < 10^{-20} \text{ m}^2$$



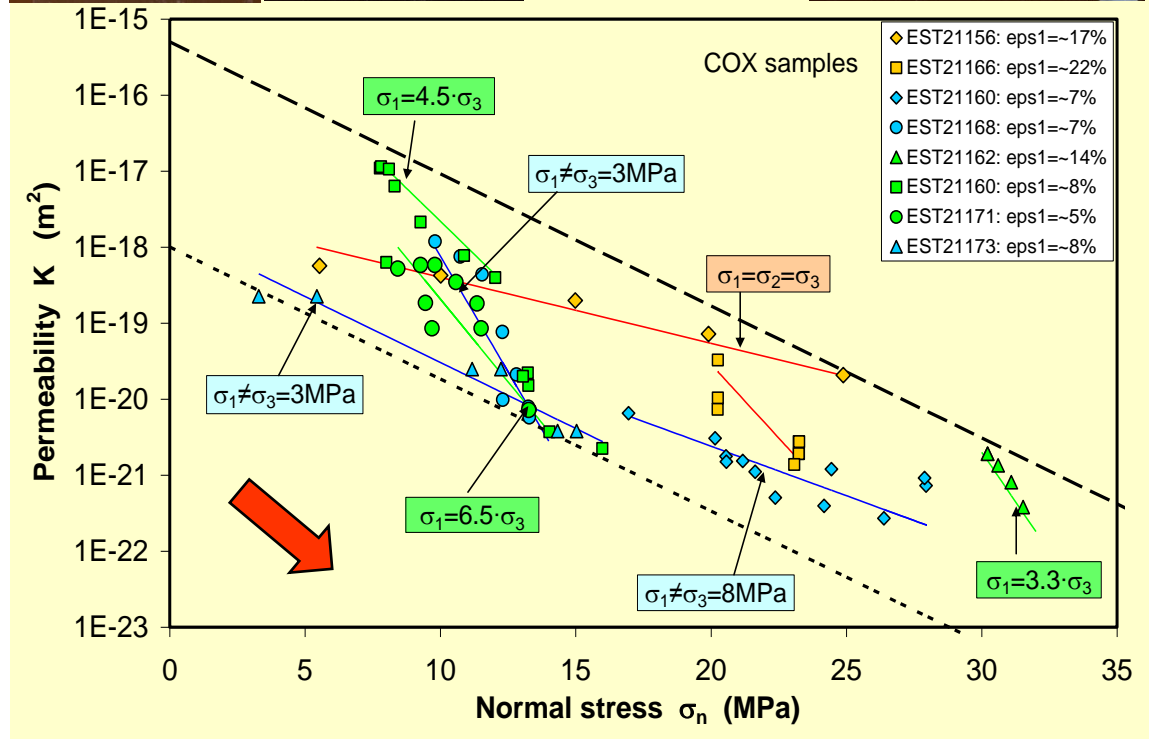
Sealing of shear fractures by compression



$\sigma_1 = \sigma_2 = \sigma_3$ ↑

$\sigma_1 = a \cdot \sigma_3$ ↑

$\sigma_3 = C, \sigma_1$ ↑



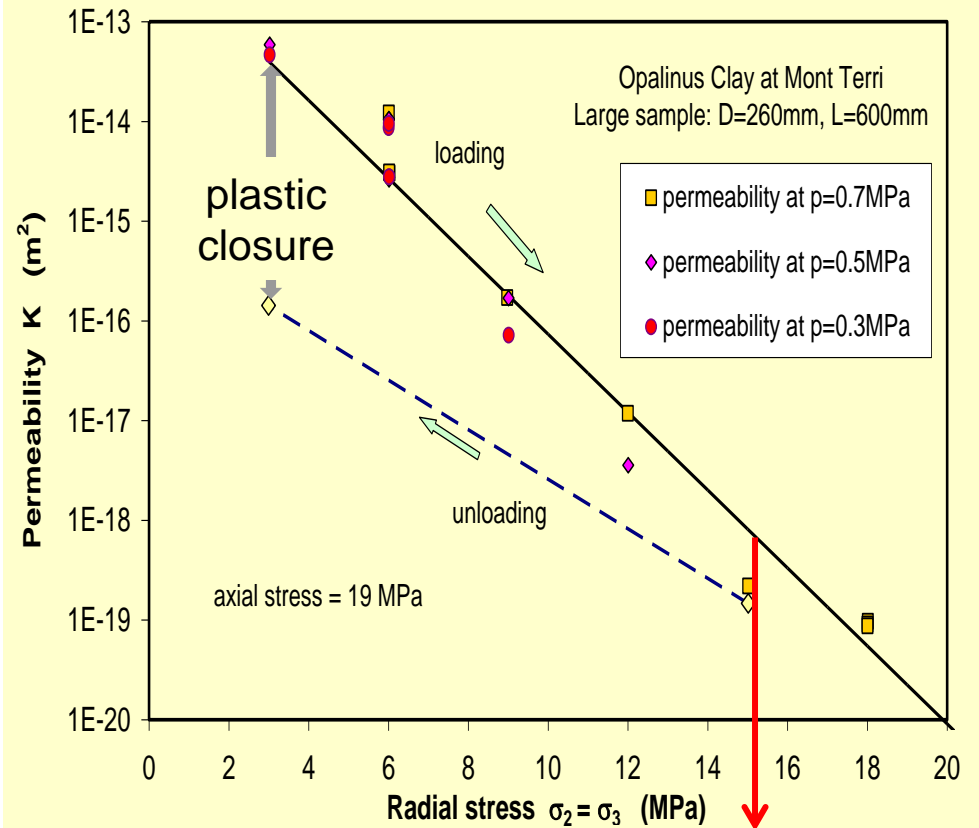
Sealing of fractures in large-scale samples

OPA sample (D260mm, L600mm)



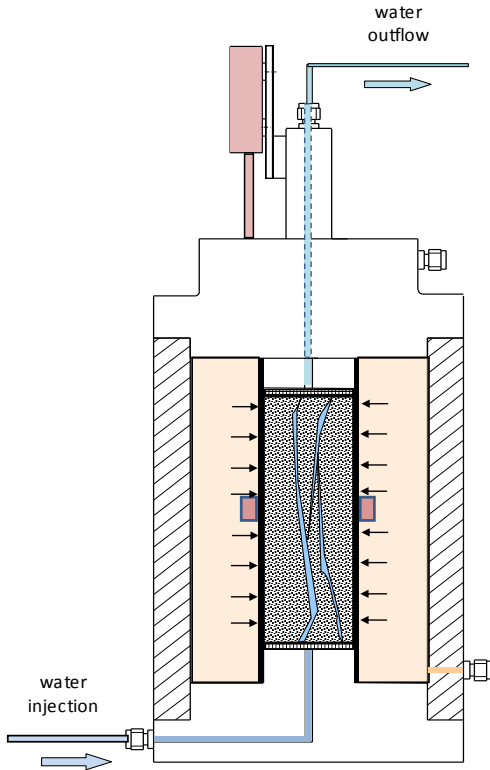
Fractures parallel to sample axis

Permeability – confining stress



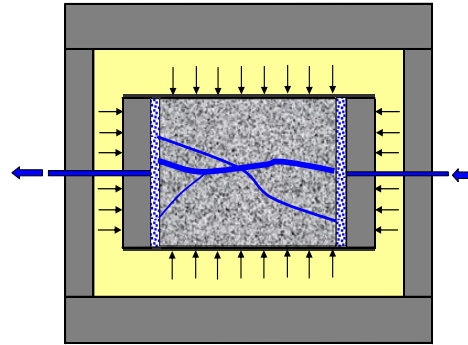
$K < 10^{-19} \text{ m}^2$ for $\sigma > 15 \text{ MPa}$

2. Water-enhanced sealing of fractures

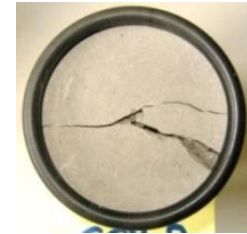


triaxial cell
fracture closure
water permeability

synthetic porewater flow



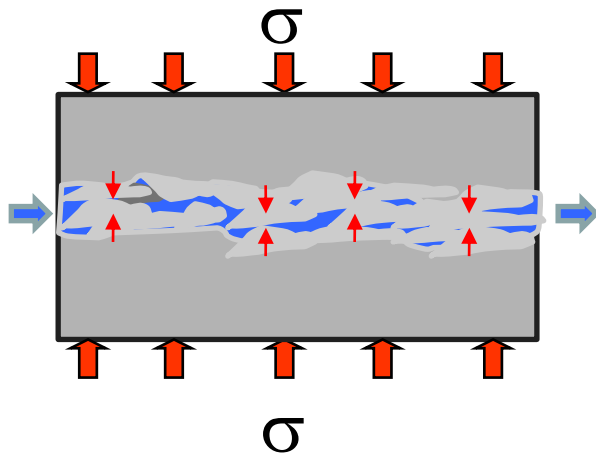
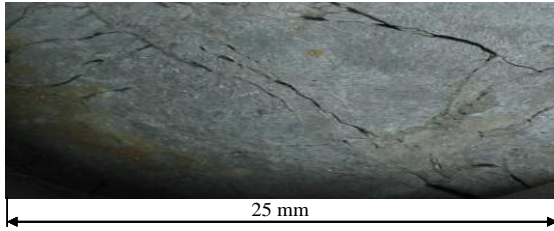
permeameters
long-term water permeability



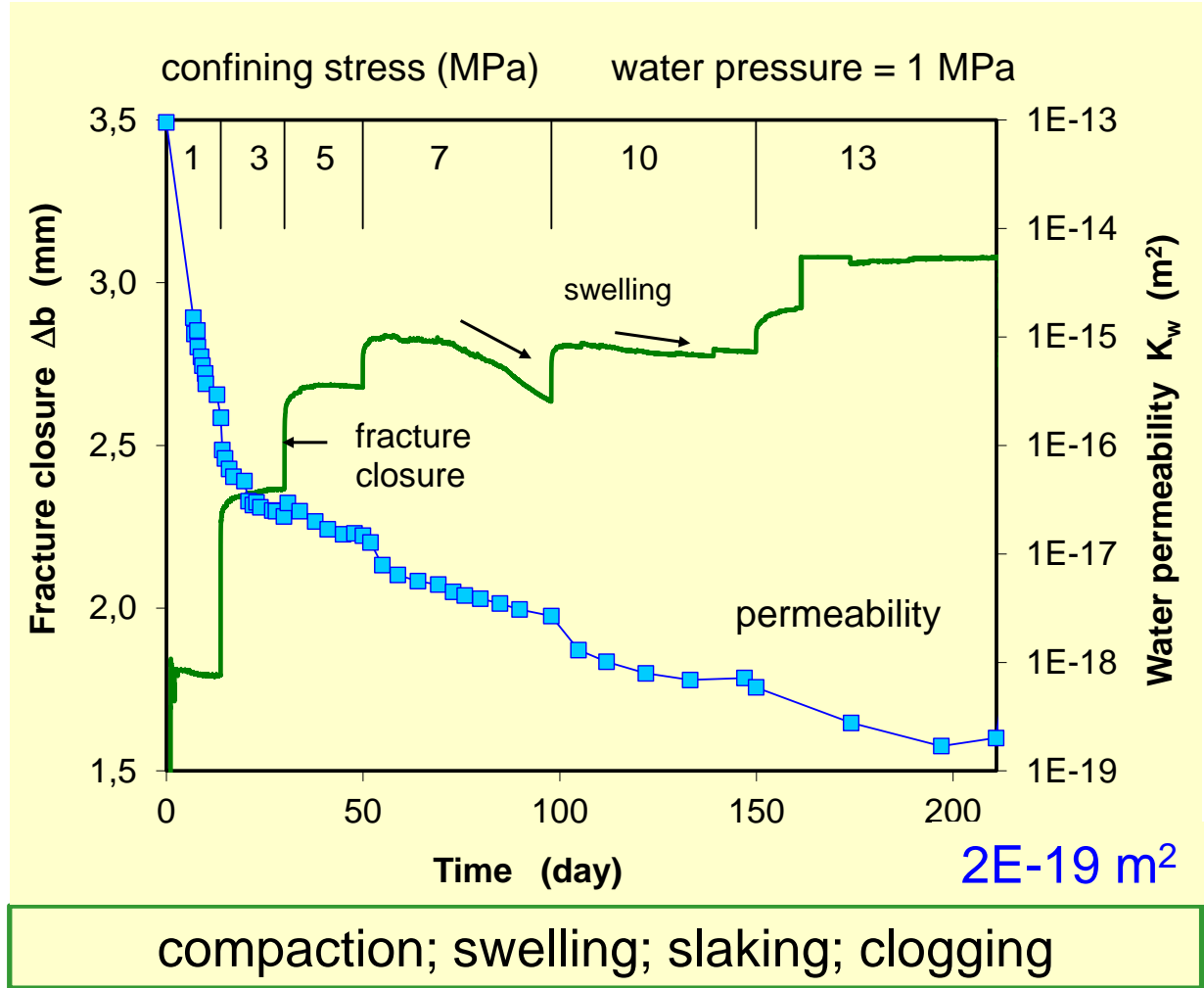
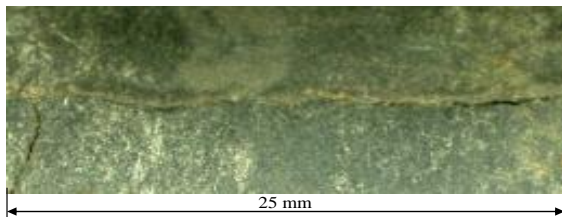
fractured samples

Fracture closure and water permeability

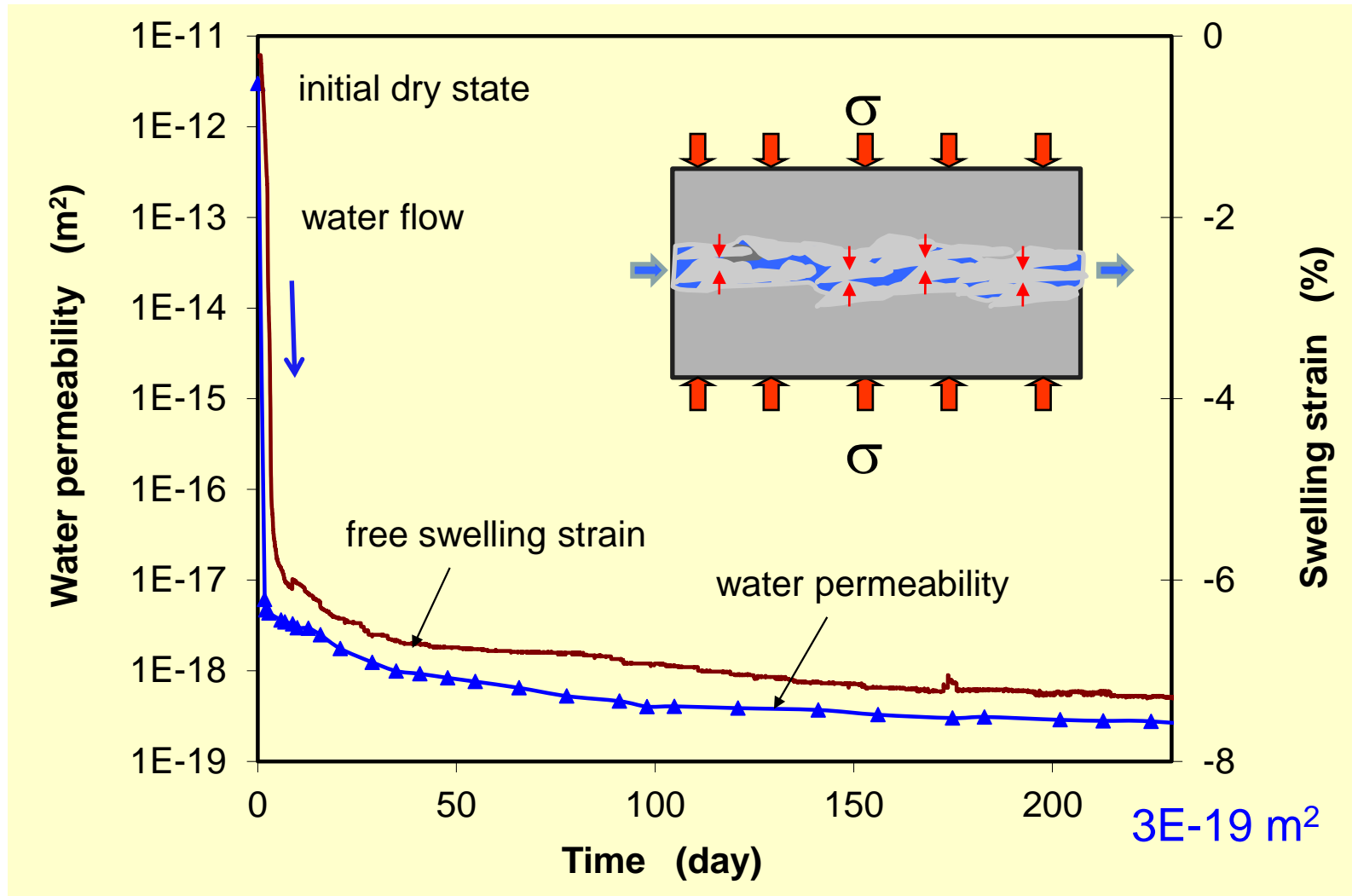
before test



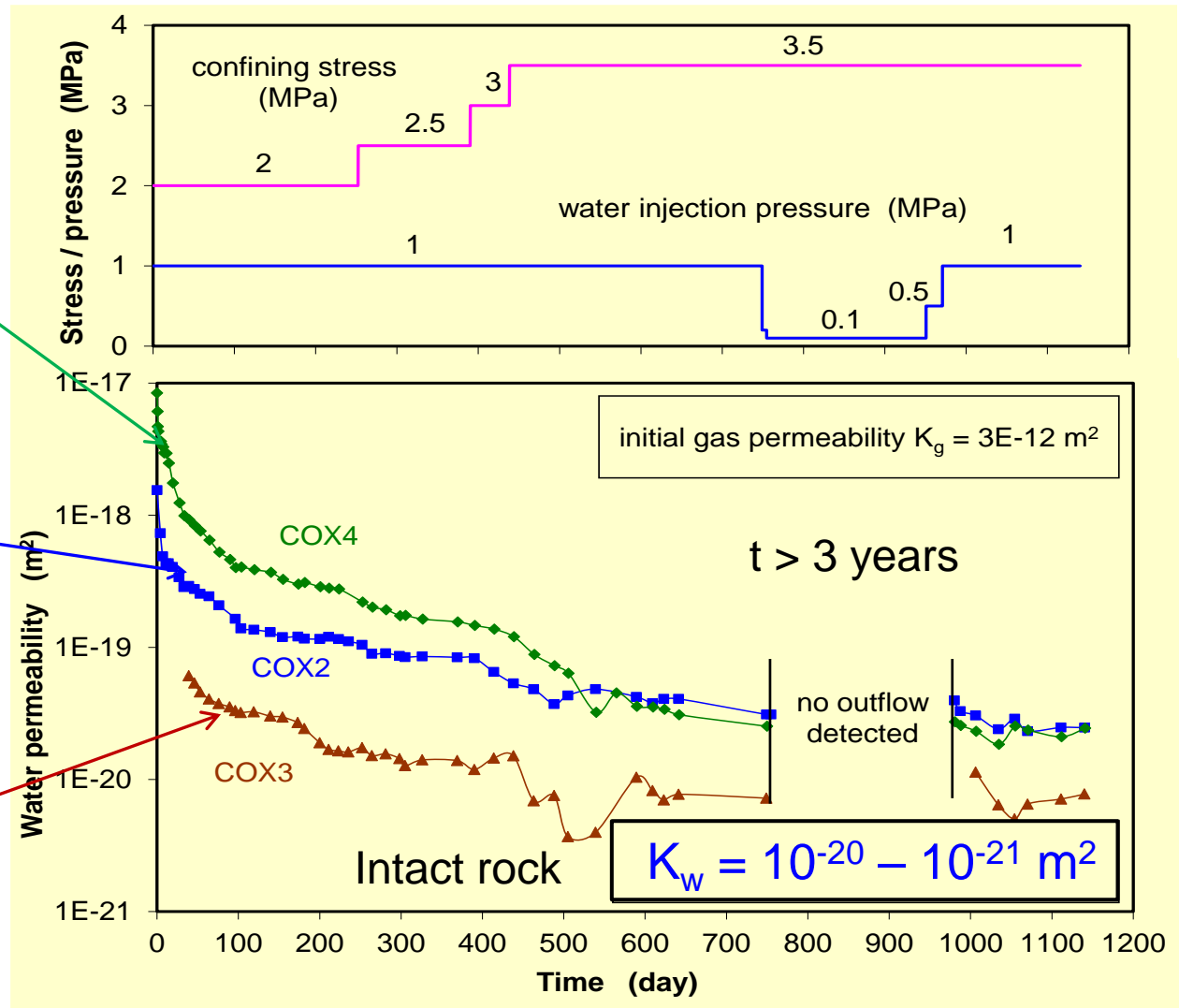
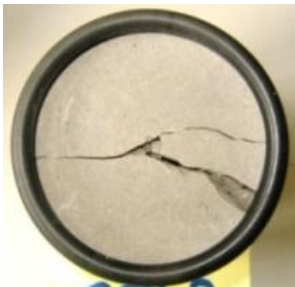
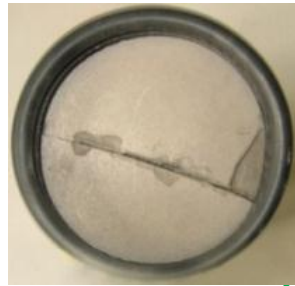
after test



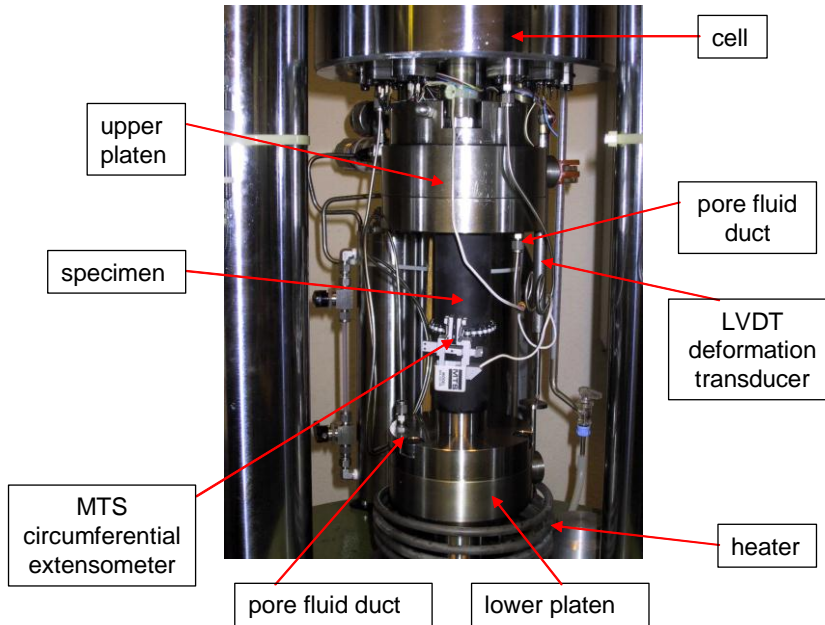
Water permeability related to clay swelling



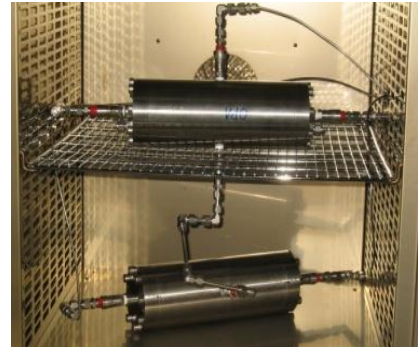
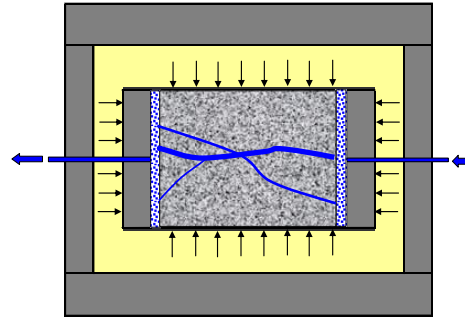
Long-term water permeability of fractured claystone



3. Thermal impact on sealing of fractures



heating in a triaxial cell
fracture closure
water permeability



heating in an oven
long-term water permeability

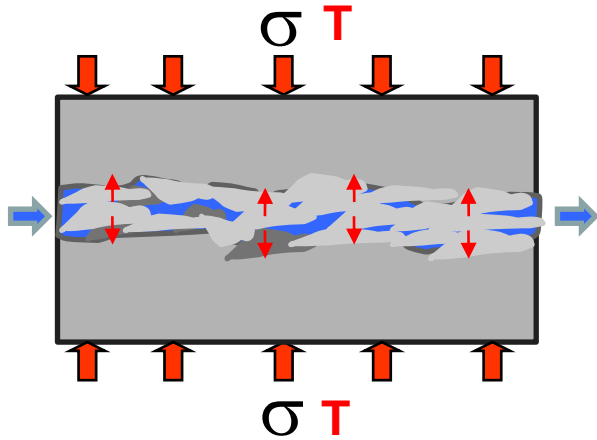


OPA sample

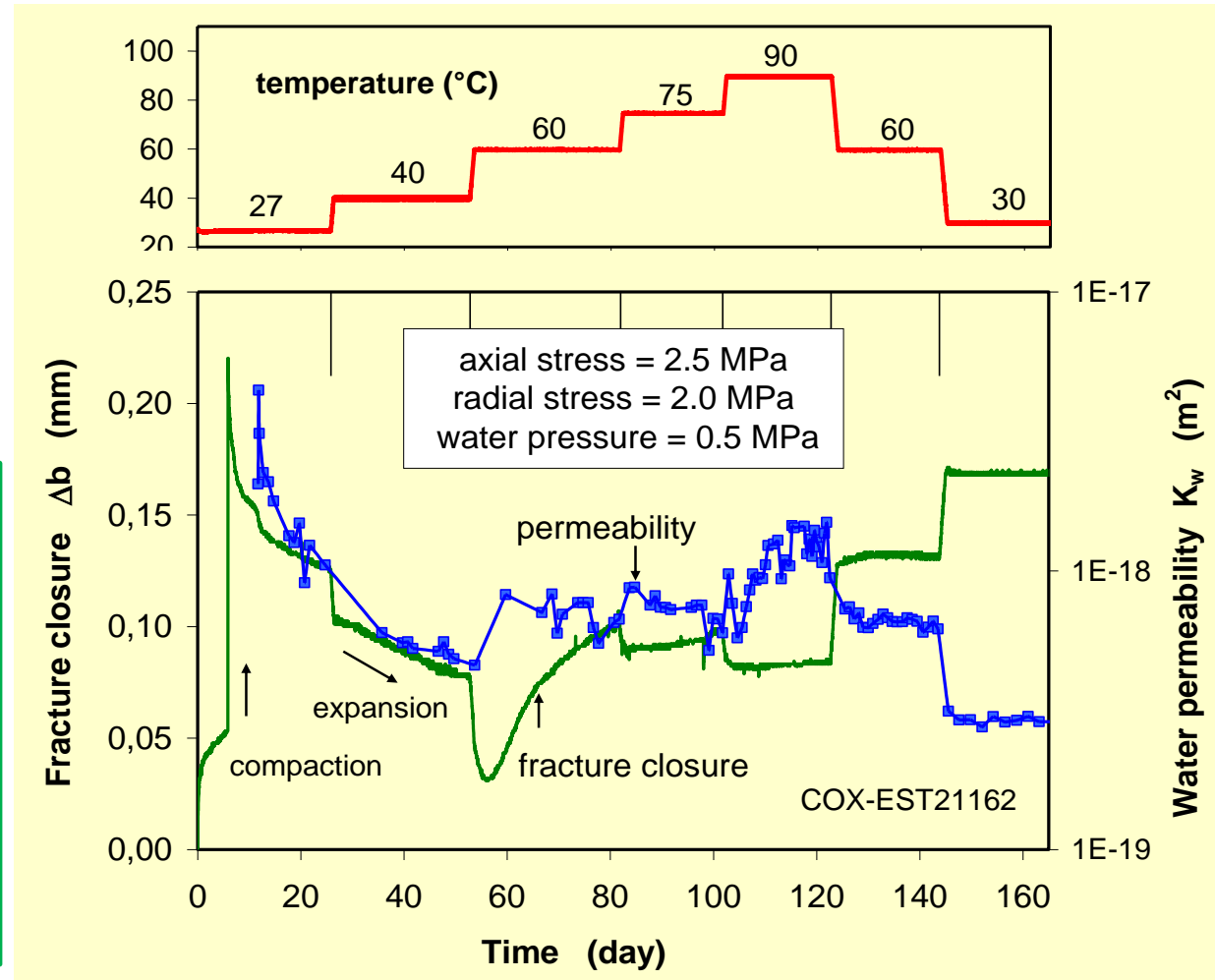


COX sample

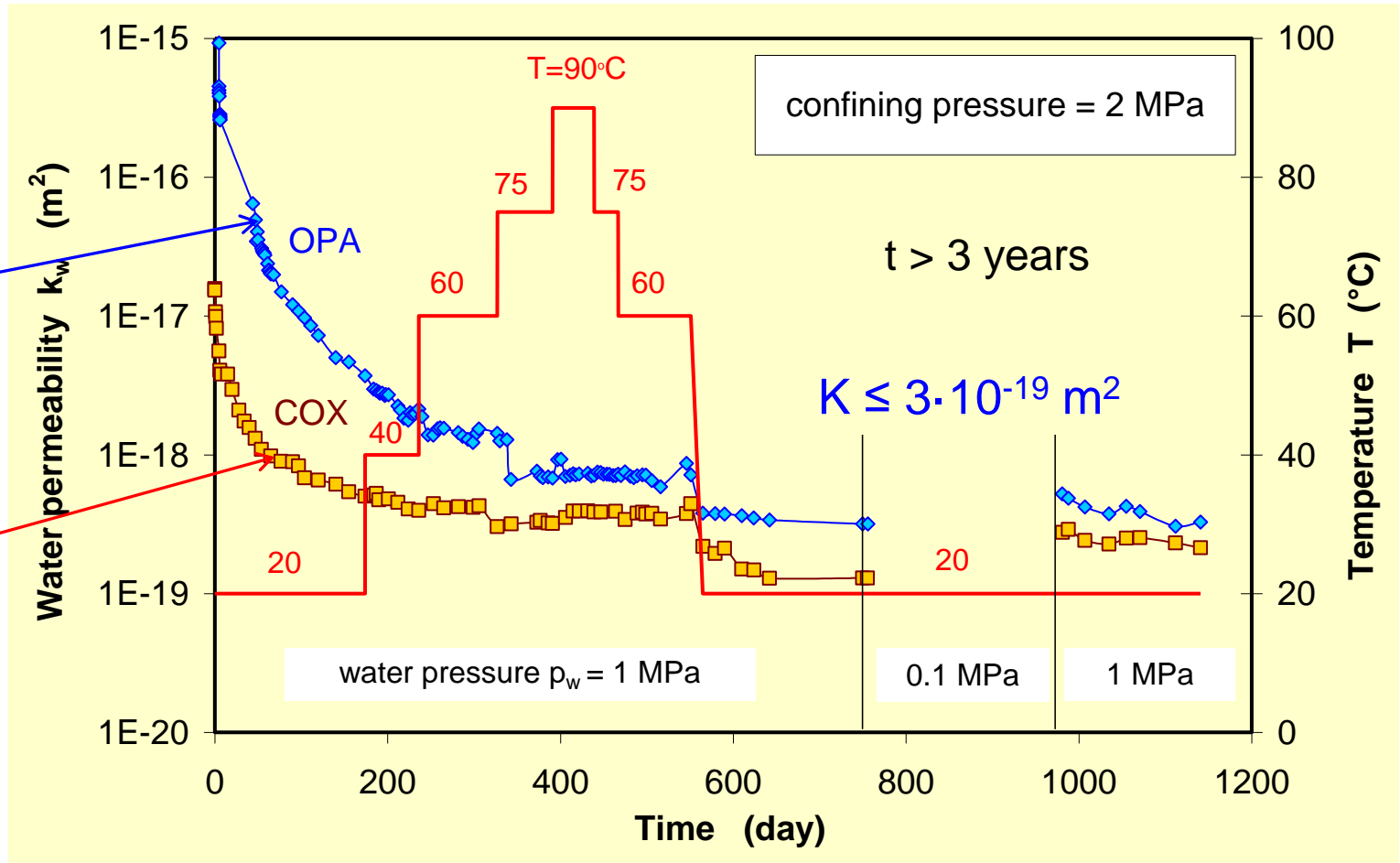
Thermal impact on fracture closure and permeability



Coupled effects:
 Mechanical compression
 Water-enhanced
 swelling/sealing
 viscosity change
 Thermal-induced
 fracture opening/closing



Long-term permeability during heating/cooling cycle



4. Simulation of EDZ-evolution around boreholes

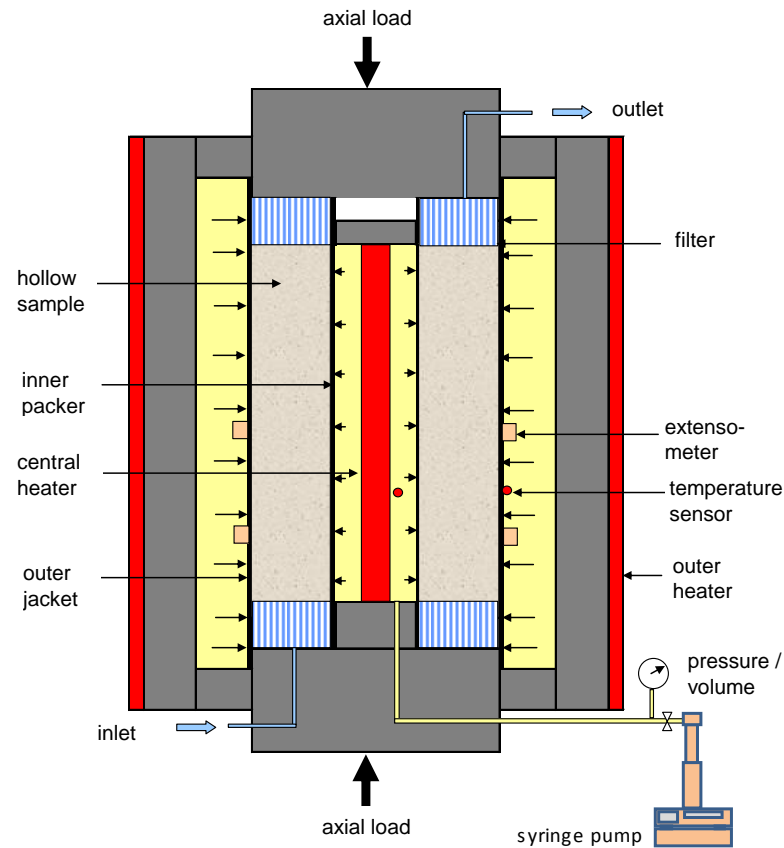
before testing



after damage



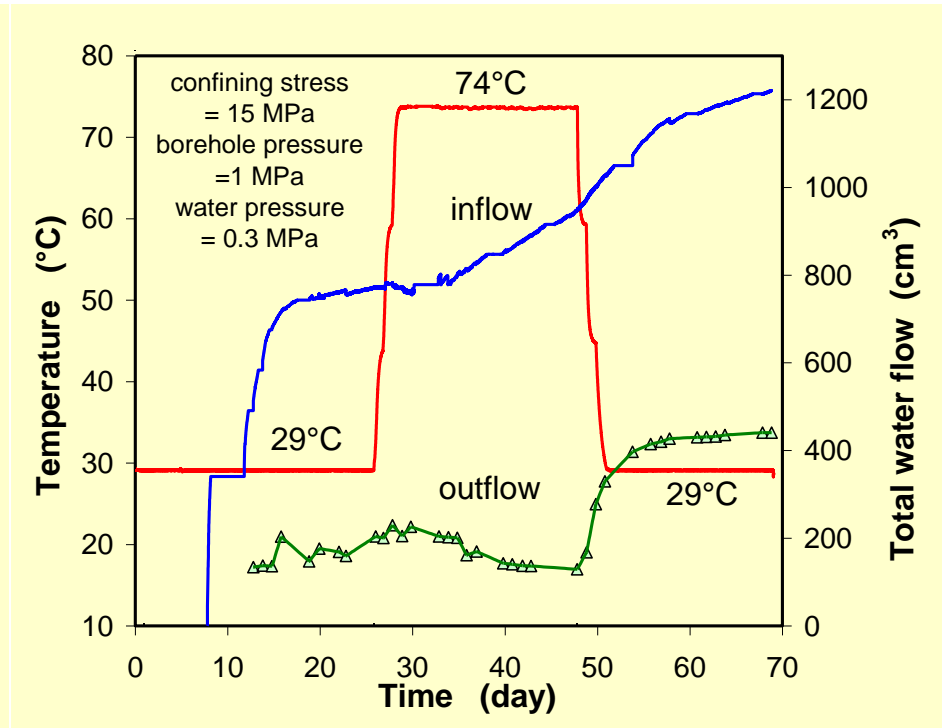
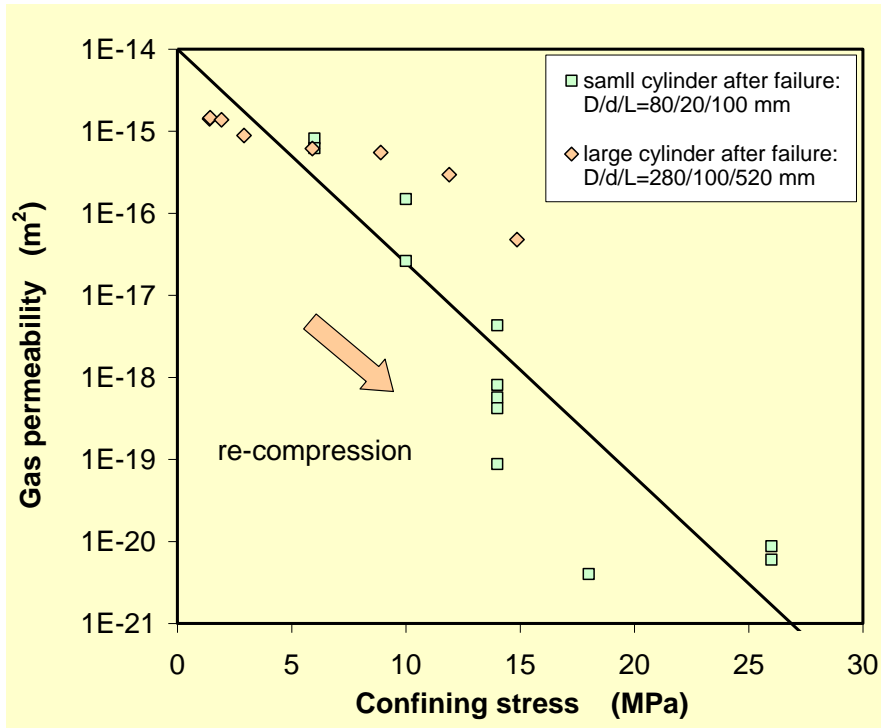
$D/L/d=280/500/100\text{mm}$



Sealing of EDZ around a borehole

gas flow by re-compaction

water flow at thermal load



$K < 10^{-19} \text{ m}^2$
for $\sigma > 15 \text{ MPa}$

before heating: $K = 2 \cdot 10^{-18} \text{ m}^2$
after heating: $K = 3 \cdot 10^{-18} \text{ m}^2$

Conclusions

- Strong experimental evidence for the high sealing capability of the studied clay rocks
- Fracture closure and permeability decrease significantly with confining stress
- Water flow enhances the sealing of fractures dramatically
- Thermal impact on the sealing of fractures insignificant
- Fractures in clay rocks can be fully re-sealed to the intact state under the repository conditions
- Models needed for prediction and assessment of the realistic sealing process of the EDZ in repositories

Acknowledgements

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Thank you for your attention !